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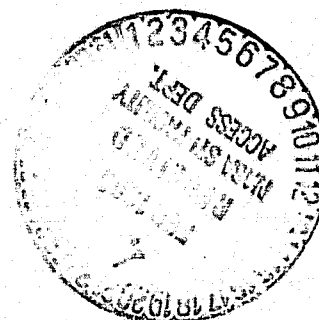
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A NUMERICAL METHOD FOR INTERFACE PROBLEMS IN ELASTODYNAMICS

By David S. McGhee
Systems Dynamics Laboratory

December 1984



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16. ABSTRACT This study deals with the numerical implementation of a formulation for a class of interface problems in elastodynamics. This formulation combines the use of the finite element and boundary integral methods to represent the interior and the exterior regions, respectively. In particular, the response of a semicylindrical alluvial valley in a homogeneous halfspace to incident antiplane SH waves is considered to determine the accuracy and convergence of the numerical procedure. Numerical results are obtained for several combinations of the incidence angle, frequency of excitation and relative stiffness between the inclusion and the surrounding halfspace. The results tend to confirm the theoretical estimates, that the convergence is of the order h^2 for the piecewise linear elements used. It is also observed that the accuracy decreases as the frequency of excitation increases or as the relative stiffness of the inclusion decreases.			
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TECHNICAL MEMORANDUM

A NUMERICAL METHOD FOR INTERFACE PROBLEMS IN ELASTODYNAMICS

I. INTRODUCTION

In ground motion studies of earthquakes, the principal interest is in the effect on a localized region of the Earth. This region can take the form of a structure foundation, a region behaving nonlinearly near a structure, or a region that has significantly different soil properties from its surroundings. The difficulty in dealing with this type of problem analytically, is the infinite nature of the Earth, in relation to the region of interest, and its energy absorbing characteristics. In order to address these problems, either very large finite element models are required or absorbing boundaries must be used. Large finite element models are computationally inefficient and standard absorbing boundaries often do not accurately represent the energy dissipation of the Earth.

This problem can be defined in terms of an interior finite region and an exterior infinite region. This type of problem is called an "Interface Problem." A method, being investigated recently, to study these problems combines finite element and boundary integral methods [1,3]. The exterior region is handled by means of a boundary integral formulation and the interior is handled with finite element methods. Continuity conditions are placed across the boundary involving the displacement field and the corresponding tractions.

In this study, this technique is applied to a specific problem. The goal is to develop a computer implementation of the method and determine its accuracy and convergence. The problem chosen is that of an anti-plane SH shear wave incident upon a semi-cylindrical alluvial valley. A closed form analytical solution for this problem is available [2] and will be the basis for the comparisons made.

The specific problem presented here is a simple one. The study, however, has two significant goals: (1) to compare the approximate method with exact analytical results, and (2) to establish a firm baseline for further extensions of the method.

II. MATHEMATICAL FORMULATION

A. Problem Formulation

In order to formulate the problem in question, the region of interest must first be defined. Consider the geometry of Figure 1. The region Ω^+ is to represent homogeneous elastic material with mass density ρ^+ and Lamé's constants λ^+ , μ^+ . The region Ω represents a possibly inhomogeneous cylinder with properties ρ^- , λ^- , and μ^- depending on the spatial coordinates x_1 and x_2 . C is a traction-free surface and Γ is the interface between Ω and Ω^+ .

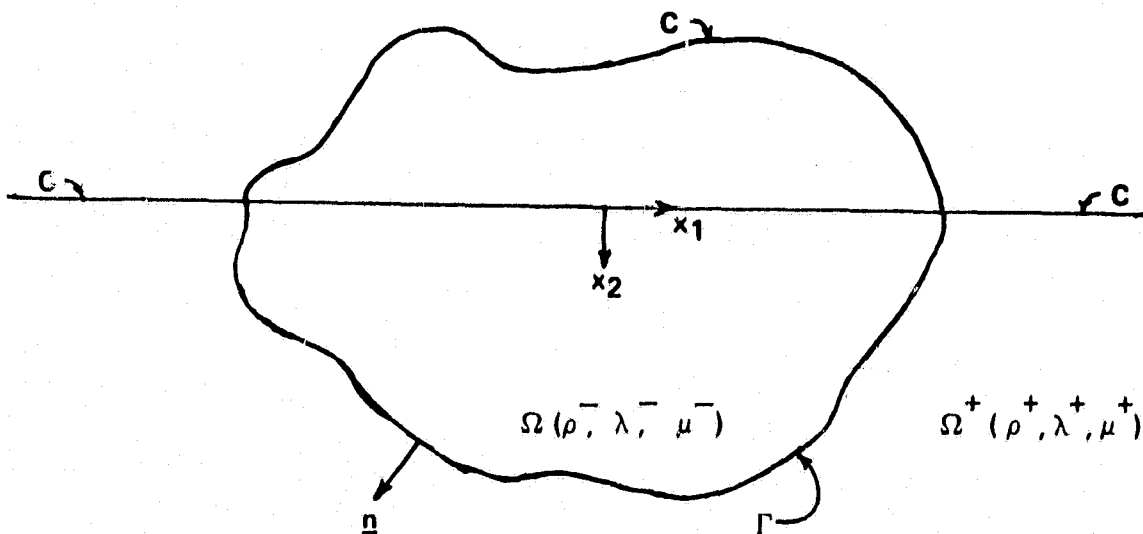


Figure 1.

A displacement field must be defined next. The case of antiplane strain due to an incoming antiplane shear wave shall be studied. While this represents a rather restricted type of excitation, the corresponding response will have qualitative similarities with that due to more general types of plane wave excitation. This approach can then be useful in gaining physical insight into the problem of evaluating the effects of local geology on ground motion.

The single non-vanishing, antiplane displacement is assumed to be time-periodic of the form:

$$W(x_1, x_2, t) = \text{Re}[w^t(x_1, x_2) e^{i\omega t}] \quad (1)$$

Also, $w^o(x_1, x_2)$ corresponds to the driving field. w^o will consist of an incoming wave defined in the halfspace $x_2 > 0$ and its reflection from the surface $x_2 = 0$, taken to be traction free. For specifying w^o it will be assumed that the entire halfspace is homogeneous, with properties equal to those of Ω^+ . That is, it will be assumed that the excitation displacement field, or free-field displacement, w^o is known in the absence of the obstacle Ω .

For convenience, a displacement w is defined such that:

$$w = \begin{cases} w^t & \text{in } \Omega \\ w^t - w^o & \text{in } \Omega^+ \end{cases} \quad (2)$$

Thus, in Ω , w represents the total displacement; that is, the displacement due to the free-field excitation, w^o , and the effects of the obstacle Ω . In Ω^+ , w represents only the effects of the obstacle Ω without the free-field excitation. In other words, in Ω^+ , w represents the scattered field only.

The problem then is to find the time periodic displacement field w , inside and outside the obstacle Ω , such that it satisfies the three following conditions. First, since both regions Ω and Ω^+ are linearly elastic, the displacement field w must satisfy a generalized, reduced wave equation in both of these regions. Second, w must satisfy several boundary conditions; namely, the displacements and tractions must be continuous across Γ and C is traction free. And third, w must satisfy a radiation condition in Ω^+ . These conditions can be expressed as follows:

$$(\mu^- w_{x_1})_{x_1} + (\mu^- w_{x_2})_{x_2} + \rho^- \omega^2 w = 0 \quad \text{in } \Omega \quad (3)$$

$$\mu^+ \nabla^2 w + \rho^+ \omega^2 w = 0 \quad \text{in } \Omega^+ \quad (4)$$

$$w^{t+} - w^{t-} = 0 \quad ; \quad \mu^+ w_n^{t+} - \mu^- w_n^{t-} = 0 \quad \text{on } \Gamma \quad (5,6)$$

$$\mu w_n = 0 \quad \text{on } C \quad (7)$$

$$w \sim r^{-1/2} e^{-ir} \quad \text{as } r = x_1^2 + x_2^2 \rightarrow \infty \quad (8)$$

where

ω = frequency of free-field motion, w°

w^{t+} = total displacement on Ω^+ side of boundary Γ

w^{t-} = total displacement on Ω side of boundary Γ

w_n^{t+} = normal derivative of total displacement on Ω^+ side of boundary Γ

w_n^{t-} = normal derivative of total displacement on Ω side of boundary Γ .

Taking equation (2) into consideration, equations (5) and (6) can be rewritten as:

$$w^- = w^+ + w^\circ \quad (9)$$

$$\mu^- w_n^- = \mu^+ w_n^+ + \mu^+ w_n^\circ \quad (10)$$

respectively, where:

w_n° = normal derivative of free-field displacement.

Equations (3), (4), (7), (8), (10), and (11) define a well-posed problem for w in Ω and Ω^+ .

It is desirable, from a computational point of view, to reformulate the problem in a way that eliminates the need to deal with an infinite exterior region, which is both time and space consuming. This is done at the expense of introducing two boundary functions on Γ . It begins with some potential theory for the Helmholtz equation:

$$\mu^+ \nabla^2 v + \rho^+ \omega^2 v = 0, \quad x_2 > 0 \quad (11)$$

subject to the radiation condition (8) and the traction-free boundary condition,

$$v_{x_2} = 0 \quad \text{on} \quad x_2 = 0.$$

G is defined by the formula:

$$G(\underline{x}, \underline{y}) = \frac{i}{H} \left\{ H_0^{(2)}(k|\underline{x}-\underline{y}|) + H_0^{(2)}(k|\underline{x}-\underline{z}^*|) \right\} \quad (12)$$

where

$$k^2 = \omega^2 \rho^+ / \mu^+$$

$$\underline{y}^* = (y_1, -y_2)$$

$H_0^{(2)}(\cdot)$ = the Hankel function of the second kind and zeroth order.

Physically, G can be interpreted as the displacement produced at \underline{x} due to a steady-state point load of frequency ω and unit amplitude at \underline{y} .

It is assumed that the solution v in Ω^+ can be represented in terms of a simple layer with density ϕ ; that is, it is assumed that a function ϕ exists, defined over Γ , such that:

$$v(\underline{x}) = \int_{\Gamma} G(\underline{x}, \underline{y}) \phi(\underline{y}) dS_{\underline{y}} \quad \text{in} \quad \Omega^+ \quad (13)$$

Thus, the displacement v at every point within Ω^+ can be represented in terms of a density function ϕ defined only on Γ . It can be shown [5] that G is a continuous function and, therefore, the limiting displacement v^{\pm} on Γ is given by

$$v^{\pm}(\underline{x}) = \int_{\Gamma} G(\underline{x}, \underline{y}) \phi(\underline{y}) dS_{\underline{y}} \quad \text{on} \quad \Gamma \quad (14)$$

In addition, under the assumption that Γ is smooth, the limiting normal derivative is [5]

$$v_n^\pm(\underline{x}) = \pm \frac{1}{2} \phi(\underline{x}) + \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{x}}} \phi(\underline{y}) dS_{\underline{y}} \quad \text{on } \Gamma. \quad (15)$$

The plus and minus denote limits from Ω^+ and Ω , respectively, and $n_{\underline{x}}$ is the unit normal vector on Γ at point \underline{x} (Fig. 1). Then equations (4), (5), and (6) can be replaced in the original problem statement by a combination of equations (9), (10), (14), and (15). This yields

$$w^- = \int_{\Gamma} G(\underline{x}, \underline{y}) \phi(\underline{y}) dS_{\underline{y}} + w^0 \quad \text{on } \Gamma$$

$$\mu^- w_n^- = \frac{1}{2} \mu^+ \phi(\underline{x}) + \mu^+ \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{x}}} \phi(\underline{y}) dS_{\underline{y}} + \mu^+ w_n^0 \quad \text{on } \Gamma.$$

In order to arrive later at a symmetric discretized formulation of the problem, the following analogues of the Helmholtz formulas are introduced. If v satisfies equations (11) and (12) in Ω then,

$$1/2 v^- = \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} v^-(\underline{y}) dS_{\underline{y}} - \int_{\Gamma} G(\underline{x}, \underline{y}) v_n^-(\underline{y}) dS_{\underline{y}} \quad \text{in } \Omega. \quad (16)$$

If v satisfies equations (11) and (8) in Ω^+ then,

$$1/2 v^+ = \int_{\Gamma} G(\underline{x}, \underline{y}) v_n^+(\underline{y}) dS_{\underline{y}} - \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} v^+(\underline{y}) dS_{\underline{y}} \quad \text{in } \Omega^+. \quad (17)$$

By equations (9) and (10) $w^+ = w^- - w^0$ and $w_n^+ = \mu^-/\mu^+ w_n^- - w^0$, respectively. By substituting these results into equation (17),

$$\begin{aligned} 1/2 w^- + \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} w^-(\underline{y}) dS_{\underline{y}} - \int_{\Gamma} G(\underline{x}, \underline{y}) \left(\frac{\mu^-}{\mu^+} w_n^- \right)(\underline{y}) dS_{\underline{y}} \\ = 1/2 w^0 - \int_{\Gamma} G(\underline{x}, \underline{y}) w_n^0(\underline{y}) dS_{\underline{y}} + \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} w^0(\underline{y}) dS_{\underline{y}}, \end{aligned} \quad (18)$$

is obtained. Now w^0 is a solution of equation (11) in Ω , hence by equation (16),

$$1/2 w^o = \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{y}} w^o(\underline{y}) dS \underline{y} - \int_{\Gamma} G(\underline{x}, \underline{y}) w_n^o(\underline{y}) dS \underline{y} .$$

So the right hand side of equation (18) becomes w^o and can be rewritten,

$$1/2 w^- + \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{y}} w^-(\underline{y}) dS \underline{y} - \int_{\Gamma} G(\underline{x}, \underline{y}) \left(\frac{\mu^-}{\mu^+} w_n^- \right) (\underline{y}) dS \underline{y} = w^o . \quad (19)$$

This leads to the following problem. Find $(w, \mu^- w_n^-, \phi)$ such that

$$(\mu^- w_{x_1})_{x_1} + (\mu^- w_{x_2})_{x_2} + \rho^- \omega^2 w = 0 \quad \text{in } \Omega \quad (20a)$$

$$w^- = \int_{\Gamma} G(\underline{x}, \underline{y}) \phi(\underline{y}) dS \underline{y} + w^o \quad \text{on } \Gamma \quad (20b)$$

$$\mu^- w_n^- = 1/2 \mu^+ \phi(\underline{x}) + \mu^+ \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{x}} \phi(\underline{y}) dS \underline{y} + \mu^+ w_n^o \quad \text{on } \Gamma \quad (20c)$$

$$\mu^- w_n = 0 \quad \text{on } C \quad (20d)$$

$$1/2 w^- + \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{y}} w^-(\underline{y}) dS \underline{y} - \int_{\Gamma} G(\underline{x}, \underline{y}) \left(\frac{\mu^-}{\mu^+} w_n^- \right) (\underline{y}) dS \underline{y} = w^o \quad \text{on } \Gamma . \quad (20e)$$

The only set of points now used are those in Ω and Γ . The set of points in Ω^+ is completely described by points in Γ by the use of the Green's function. It has been shown in Reference 1 that this problem has, in general, a unique solution provided certain critical values of ω are excluded.

B. Variational Principle

Now standard Galerkins' ideas are used to obtain a variational formulation which will be suitable for discretization by the finite element method. First, multiply equation (20a) by a test function δw and integrate over Ω using the divergence theorem and equation (20d). The result is,

$$-\int_{\Omega} \{ \mu^- (w_{x_1} \delta w_{x_1} + w_{x_2} \delta w_{x_2}) - \omega^2 \rho^- w \delta w \} dx + \int_{\Gamma} \mu^- w_n^- \delta w dS = 0 \quad (21a)$$

Next, multiply equation (20b) by a test function $\delta \mu^- w_n^-$ and integrate over Γ ;

$$\int_{\Gamma} \left[\int_{\Gamma} G(\underline{x}, \underline{y}) \phi(\underline{y}) dS_{\underline{y}} - w^-(\underline{x}) + w^0(\underline{x}) \right] \delta \mu^- w_n^-(\underline{x}) d\underline{x} . \quad (21b)$$

Perform similar calculations for equations (20c) and (20e) and combine the resulting equations linearly with (21a) and (21b) to obtain:

$$\begin{aligned} & \left[- \int_{\Omega} \{ \mu^-(w_{x_1} \delta w_{x_1} + w_{x_2} \delta w_{x_2}) - \omega^2 \rho^- w \delta w \} d\underline{x} + \int_{\Gamma} \mu^- w_n^- \delta w dS \right] \\ & - 1/2 \left[\int_{\Gamma} \left\{ \int_{\Gamma} G(\underline{x}, \underline{y}) \phi(\underline{y}) dS_{\underline{y}} - w^-(\underline{x}) + w^0(\underline{x}) \right\} \delta \mu^- w_n^-(\underline{x}) dS \right] \\ & + 1/2 \left[\int_{\Gamma} \left\{ 1/2 \mu^+ \phi(\underline{x}) + \mu^+ \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{x}}} \phi(\underline{y}) dS_{\underline{y}} + \mu^+ w_n^0 - \mu^- w_n^- \right\} \delta w^- dS \right] \\ & + 1/2 \left[\int_{\Gamma} \left\{ 1/2 \mu^+ w^-(\underline{x}) + \mu^+ \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} w^-(\underline{y}) dS_{\underline{y}} - \int_{\Gamma} G(\underline{x}, \underline{y}) (\mu^- w_n^-)(\underline{y}) dS_{\underline{y}} \right. \right. \\ & \left. \left. - \mu^+ w^0 \right\} \delta \phi(\underline{x}) dS \right] = 0 . \quad (22) \end{aligned}$$

The problem is now in a form suitable for finite element approximation. This is done by defining the various functions in equation (22) using finite element shape functions as follows:

$$w(\underline{x}) = [N(\underline{x})]^T \{w\} = [N_{\Omega}(\underline{x})^T : N_{\Gamma}(\underline{z})^T] \begin{Bmatrix} w_{\Omega} \\ w_{\Gamma} \end{Bmatrix} . \quad (23a)$$

$$\phi(\underline{x}) = [Q(\underline{x})]^T \{\phi\} \quad (23b)$$

$$\mu^- w_n^-(\underline{x}) = \lambda(\underline{x}) = [Q(\underline{x})]^T \{\lambda\} . \quad (23c)$$

The corresponding test functions are defined using the same shape functions.

Using these shape functions equation (22) leads to the matrix equation:

$$\begin{bmatrix} K_{\Omega\Omega} & K_{\Omega\Gamma} & 0 & 0 \\ K_{\Gamma\Omega} & K_{\Gamma\Gamma} & A^T & B^T \\ 0 & A & 0 & C^T \\ 0 & B & C & 0 \end{bmatrix} \begin{Bmatrix} w_{\Omega} \\ w_{\Gamma} \\ \lambda \\ \phi \end{Bmatrix} = \begin{Bmatrix} 0 \\ f_{\Gamma} \\ f_{\lambda} \\ f_{\phi} \end{Bmatrix} \quad (24)$$

where

$$\begin{aligned} [K] &= - \int_{\Omega} \{ [N_{x_1}] \mu^- [N_{x_1}]^T + [N_{x_2}] \mu^- [N_{x_2}]^T - \omega^2 [N]^T \rho^- [N] \} d\mathbf{x} \\ [A] &= 1/2 \int_{\Gamma} [Q] [N_{\Gamma}]^T dS \\ [B] &= 1/2 \mu^+ \left\{ 1/2 \int_{\Gamma} [Q] [N_{\Gamma}]^T dS + \int_{\Gamma} \int_{\Gamma} [Q] \left[\frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{y}} \right] [N_{\Gamma}]^T dS_{\underline{y}} dS \right\} \\ [C] &= - 1/2 \int_{\Gamma} \int_{\Gamma} [Q] [G(\underline{x}, \underline{y})] [Q]^T dS_{\underline{y}} dS \\ \{f_{\Gamma}\} &= - 1/2 \mu^+ \int_{\Gamma} [N_{\Gamma}] w_n^{\circ} dS \\ \{f_{\lambda}\} &= 1/2 \int_{\Gamma} [Q] w^{\circ} dS \\ \{f_{\phi}\} &= 1/2 \mu^+ \int_{\Gamma} [Q] w^{\circ} dS \end{aligned}$$

The complete development of equation (24) from equation (22) is shown in Appendix A.

For convenience $\{\lambda\}$ and $\{\phi\}$ are now condensed out, so the equation is in terms of $\{w\}$ only.

$$\begin{bmatrix} K_{\Omega\Omega} & K_{\Omega\Gamma} \\ K_{\Gamma\Omega} & K_{\Gamma\Gamma} + D_{\Gamma\Gamma} \end{bmatrix} \begin{Bmatrix} w_{\Omega} \\ w_{\Gamma} \end{Bmatrix} = \begin{Bmatrix} 0 \\ F_{\Gamma} \end{Bmatrix} \quad (25)$$

is obtained where

$$[D_{\Gamma\Gamma}] = -[A]^T [C]^{-1} [B] - [B]^T [C^T]^{-1} [A]$$

$$\{F_{\Gamma}\} = \{f_{\Gamma}\} - [A]^T [C]^{-1} \{f_{\phi}\} - [B]^T [C^T]^{-1} \{f_{\lambda}\}$$

From equation (24), it can be seen that $[K]$ is essentially the stiffness matrix of the cylinder; that is, the force at some point in the cylinder due to a unit displacement at some other point in the cylinder. $[C]$ represents the discretized compliance of the halfspace. $[A]$ and $[B]$ are matrices which couple the cylinder boundary and the halfspace boundary and guarantee the continuity of displacements and tractions across Γ .

From equation (25), $[D_{\Gamma\Gamma}]$ is the force at a point on the boundary due to a force or traction applied at some other point on the boundary allowing for the presence of the halfspace medium. $[D_{\Gamma\Gamma}]$ is essentially a representation of a nonlocal absorbing boundary developed from a Green's function rather than a spring and dash-pot model.

III. APPLICATIONS

The primary objective of this study was to develop a computer code to implement the previously described formulation and to check its accuracy. In order to do this, a baseline reference was needed. The most commonly cited problem of this type deals with a semicircular deposit with homogeneous material properties, for which an exact solution is available [2]. The program developed, therefore, used these characteristics. Extensions to more general problems can be made once the method has been checked.

The free-field antiplane shear wave, w^o , was taken as

$$w^o(x_1, x_2) = e^{-i(\omega t - kx_1 \sin \theta_0)} \cos(kx_2 \cos \theta_0) \quad (26)$$

where

θ_0 = angle of incidence

$$k^2 = \omega^2 \rho^+ / \mu^+ .$$

Figure 2 illustrates x_1 , x_2 , and θ_0 and their sign conventions.

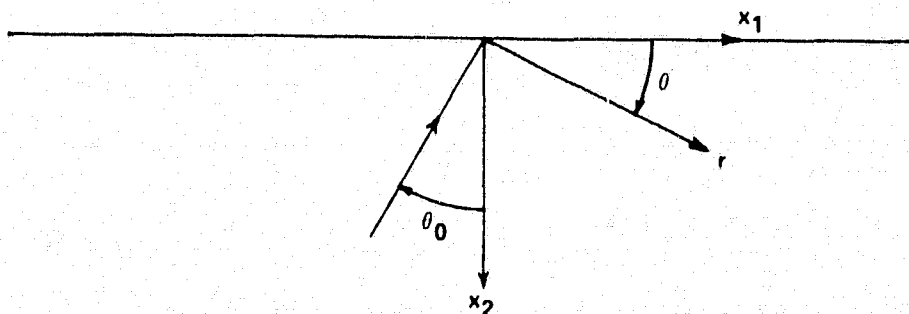


Figure 2.

With the geometry being circular, polar coordinates were used for their convenience. By substituting polar coordinates and simplifying, the incident wave becomes:

$$w^o = e^{-i\omega t} \frac{1}{2} [e^{i kr \sin(\theta+\theta_o)} + e^{-i kr \sin(\theta-\theta_o)}] \quad (27)$$

and the normal derivative:

$$\frac{\partial w^o}{\partial n} = \frac{\partial w^o}{\partial r} = e^{i\omega t} \frac{1}{2} [i k \sin(\theta+\theta_o) e^{i kr \sin(\theta+\theta_o)} - i k \sin(\theta-\theta_o) e^{-i kr \sin(\theta-\theta_o)}] \quad (28)$$

The Green's function (12) can be expressed as

$$G(\underline{x}, \underline{y}) = \frac{i}{4} H_o^{(2)} [2 kr \left| \sin \frac{\Delta \theta}{2} \right|] \quad (29)$$

where

$\Delta \theta$ = angular distance between \underline{x} and \underline{y} .

Note that this form of the Green's function satisfies the wave equation in Ω^+ and the radiation condition. The normal derivative of this function is:

$$\frac{\partial G(\underline{x}, \underline{y})}{\partial n} = \frac{\partial G(\underline{x}, \underline{y})}{\partial r} = \frac{-ik}{2} H_1^{(2)} (2kr \left| \sin \frac{\Delta \theta}{2} \right|) \left| \sin \frac{\Delta \theta}{2} \right| \quad (30)$$

which is bounded and continuous.

For the interior region the elements used for the finite element analysis represent a simple polar grid as shown in Figure 3. This necessitated two basic elements; a "triangular" element and a "rectangular" element. For this interior region the displacement was approximated by shape functions which are piecewise linear in both r and θ . This choice of shape functions provided the necessary accuracy but kept the computations simple.

The boundary elements of the halfspace for the functions ϕ and λ are "line" elements. To preserve symmetry of the resulting matrices, these two functions used the same shape function. A piecewise constant shape function was chosen here, again because this provided the necessary accuracy while keeping computations simple. These elements were chosen to coincide with the boundary elements resulting from the interiors division. This is not necessary to the method but is more convenient computationally.

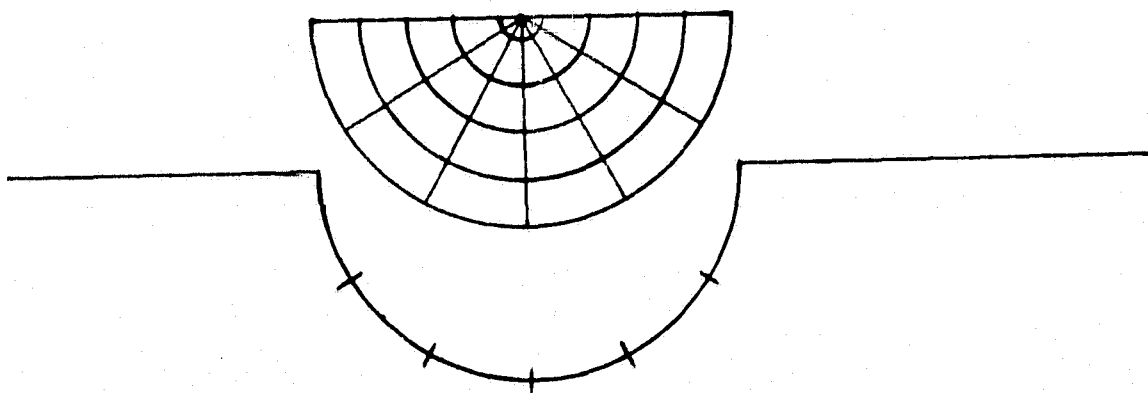


Figure 3.

In the interior, the number of elements in the radial and angular directions was varied to provide a check of the convergence rate of the method. Although it resulted in elements of significantly different areas, the radial divisions were made uniform. This resulted in a natural placing of more elements where needed, near the center. The maximum number of elements used for this study was dictated by the limits of the computer used.

The most computationally expensive parts of this method are the integrals involving the Green's function and its normal derivative. Because of their complexity, these integrals must be evaluated numerically. Gaussian quadrature was selected for this purpose. Because the integrand contains a logarithmic singularity, a modified Gaussian method, to take directly into effect this singularity, was used as presented by Harris and Evans [4]. In addition, care was taken to split the integral, at the singularity, into two integrals. The integration schemes used were tested on the natural logarithm function to determine the number of points necessary for accuracy. By using these techniques the amount of computation for each integral was kept to a minimum while returning the necessary accuracy.

The symmetry of the full space problem was also used to reduce the number of computations. By constructing the matrices for the full space the actual number of integrals necessary to perform was reduced because of symmetry. Further symmetry considerations then allowed the matrices to be reduced to the halfspace problem.

For the various matrix operations, such as solving equations and inverting matrices, the appropriate IMSL routines were used.

IV. NUMERICAL RESULTS

As stated previously, the primary objectives of this study were to determine the accuracy and convergence of the proposed formulation. Given the applications discussed in Section III a number of cases were considered.

The first consideration was the number of elements needed to achieve a desired accuracy and the rate of convergence as the number of elements is increased. For this study, results were computed for five radial and five angular elements; 10 radial and 10 angular elements; and 20 radial and 20 angular elements.

The second consideration was the frequency of the free-field motion. As the frequency of the free-field motion increases, it was expected that the smoothness of the response would decrease. This indicates that more elements are needed to achieve a fixed accuracy for higher frequencies. The circular dimensionless frequencies considered in this study were π , 0.50π , and 0.25π .

The third consideration was the angle of incidence of the free-field wave front. It was of interest to determine whether the angle of incidence has any effect on the solution. To do this, this study computed results for incidences of 0° and 60° . This represented wave fronts coming from directly below and from the left, respectively.

The fourth consideration was the stiffness of the obstacle. The ability to vary the stiffness of the obstacle in relation to the stiffness of the halfspace is important to the usefulness of the formulation and any further extensions. For this study two cases were considered. An obstacle stiffer than the halfspace was studied using a ratio of mass densities (ρ^-/ρ_+) equal to 1.50 and a ratio of shear wave velocities (β^-/β_+) equal to 2.00. A softer obstacle used a density ratio of 0.67 and a velocity ratio of 0.50.

For all of the above applications and cases a closed form solution is available in terms of a series involving Bessel functions [2]. All of these cases and their exact solutions were computed. The results for various points on the surface ($\theta = 0^\circ$ and $\theta = 180^\circ$) were compiled into Tables 1 through 3. Both the real and imaginary parts of the solution are shown. For an incidence angle of 0° only those points where $\theta = 0^\circ$ are shown since the response is symmetric.

The relative errors for three surface points were computed and plotted against the number of elements for the various cases. This error is defined as:

$$\text{error} = \left| \frac{\text{exact} - \text{computed}}{\text{exact}} \right|$$

The graphs of the errors are shown in Figures 4 through 9.

As can be seen from the graphs, the convergence and accuracy of the formulation is very good. The rate of convergence is on the order of the square of the number of elements or better. The relative error itself is small even when only using 20 elements. The effect of frequency generally follows the expected trend, that is, as the frequency increases more elements are needed to provide accurate answers. There is little effect on the accuracy of the formulation from the angle of incidence of the free-field motion or the relative stiffness of the obstacle and halfspace.

Another concern was the viability of the formulation at or near the natural frequency of the obstacle when having the same material properties as the exterior region. At this natural frequency, the matrix [C] defined in equation (24) becomes ill-conditioned and difficult to invert. This is a particular problem with this study since inversion of the [C] matrix was required for the reduction done in equation (25). This inversion did, in fact, fail at the natural frequency of 0.7655π . However, good results were obtained at a frequency of 0.7632π . Results for this frequency and

another close frequency are shown in Table 4. It is believed that this problem can be avoided by solving the full problem [equation (24)]. This could not be confirmed in this study, however, because of computer limitations.

V. CONCLUSIONS

The numerical results obtained indicate the formulation is very good. Accuracy is good even with few elements and the convergence rates are on the order of the number of elements squared or better. The formulation can be used for a wide range of incidence angles and frequencies. A variety of obstacle densities can be accommodated and the natural frequency of the halfspace can be closely approached.

Now that the formulation has been numerically proven, a number of extensions for further study suggest themselves. An obstacle of inhomogeneous properties, a region of irregular shape, and a region of nonlinear properties are some possible extensions. This study provides a firm baseline for this further study.

RADIUS = 0.0

$P-/P+ = 0.67$

$B-/B+ = 0.50$

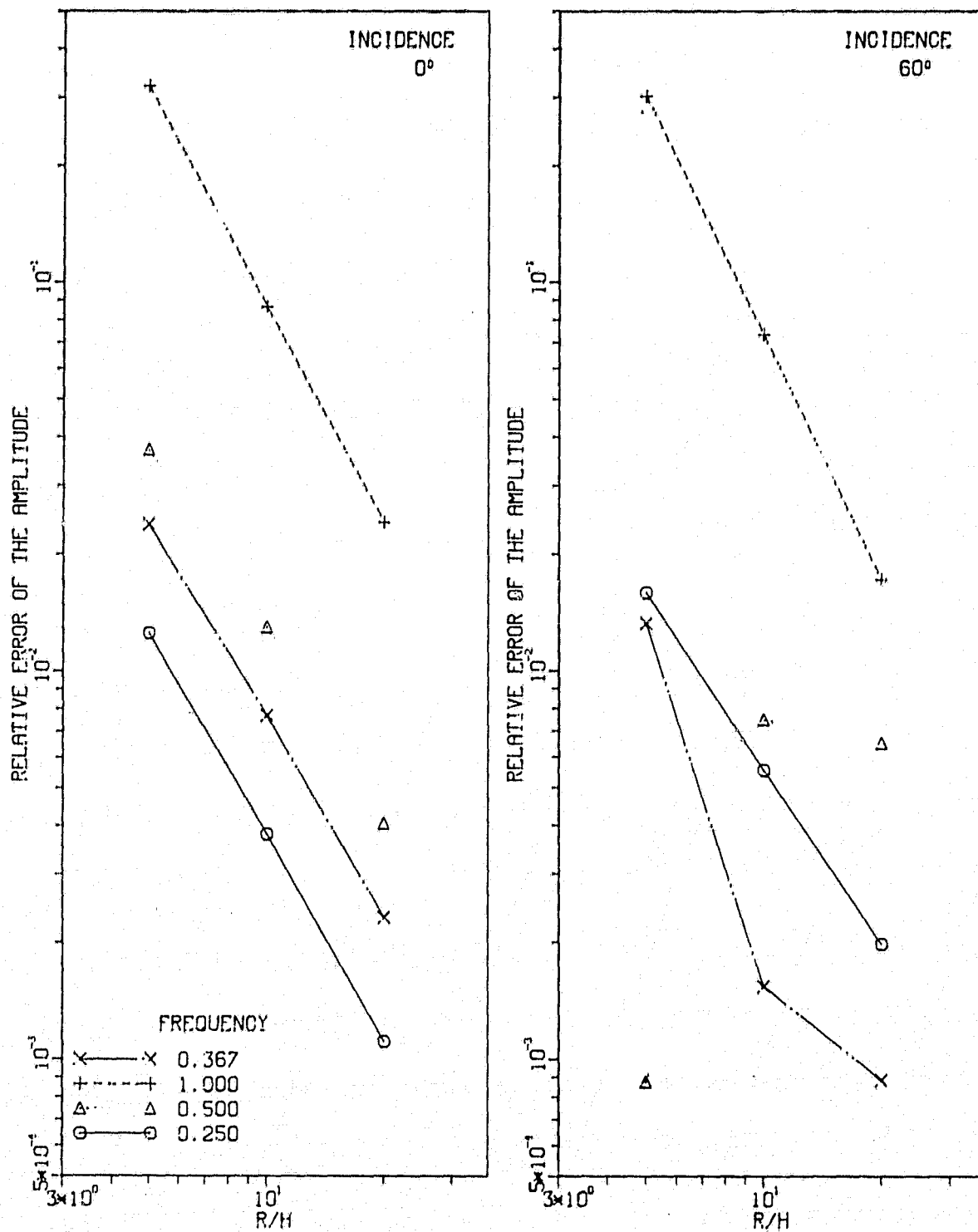


Figure 4.

RADIUS = -0.4

$P-/P+ = 0.67$

$B-/B+ = 0.50$

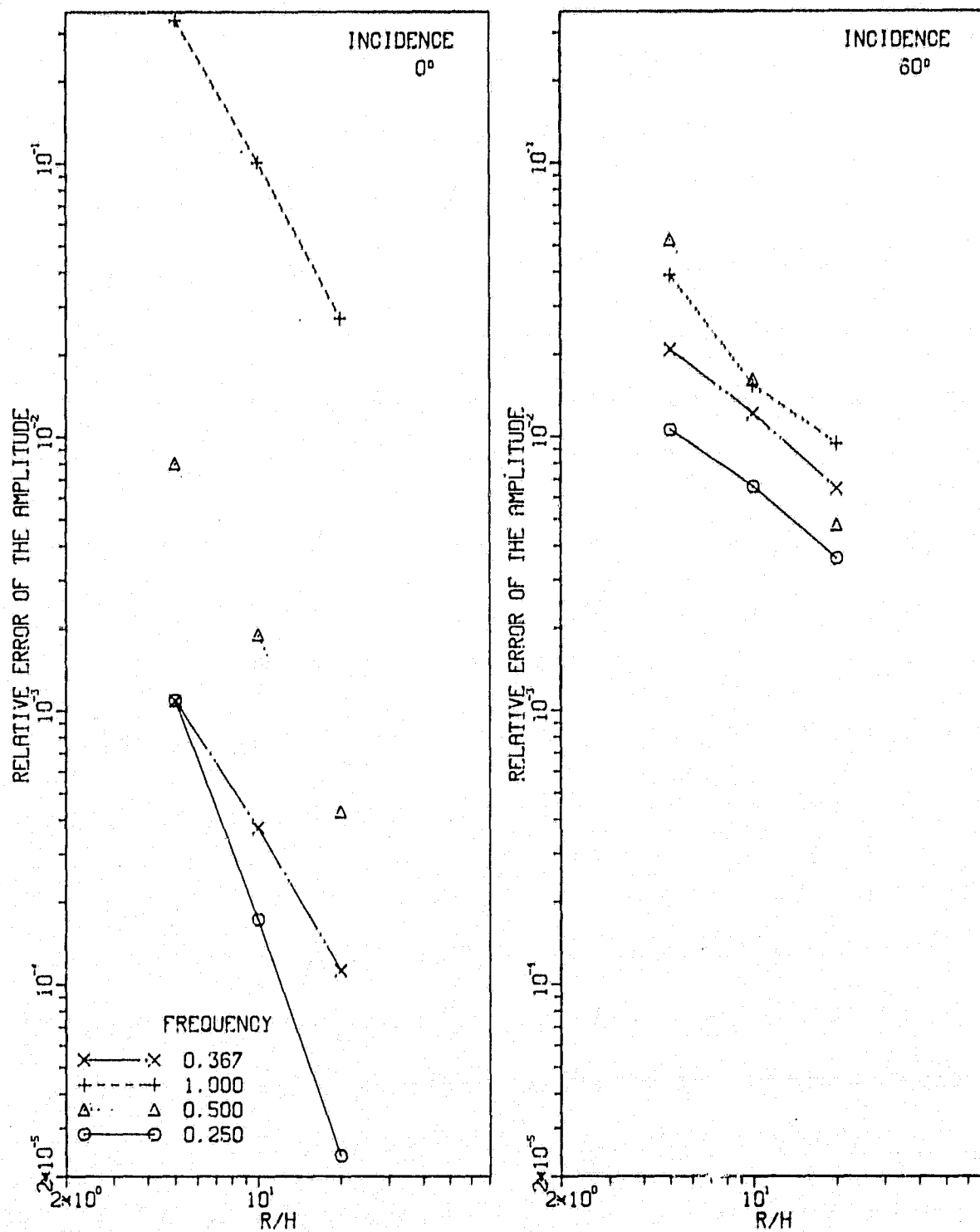


Figure 5.

RADIUS = 0.8

P-/P+ = 0.67

B-/B+ = 0.50

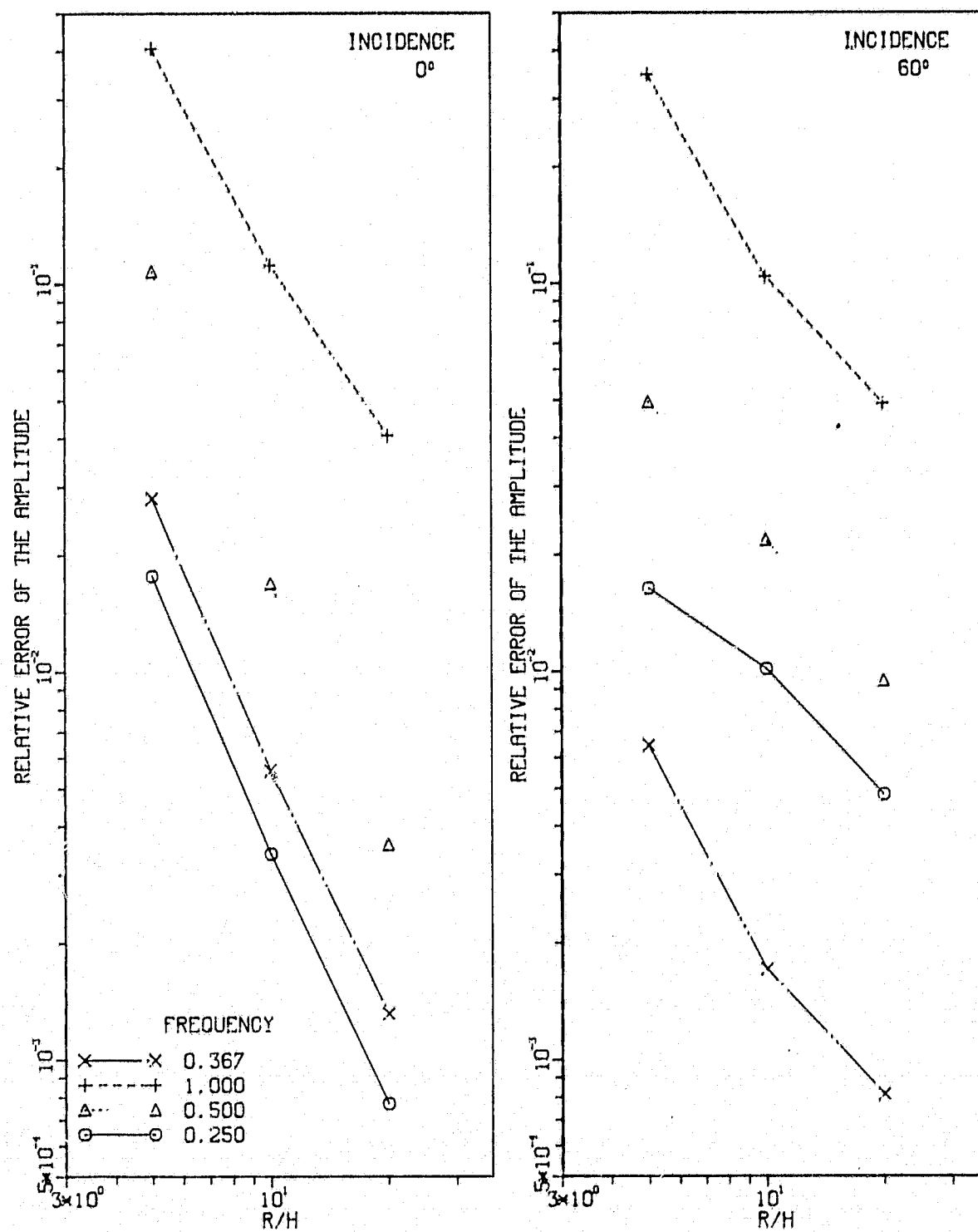


Figure 6.

RADIUS = -0.4

P-/P+ = 1.50

B-/B+ = 2.00

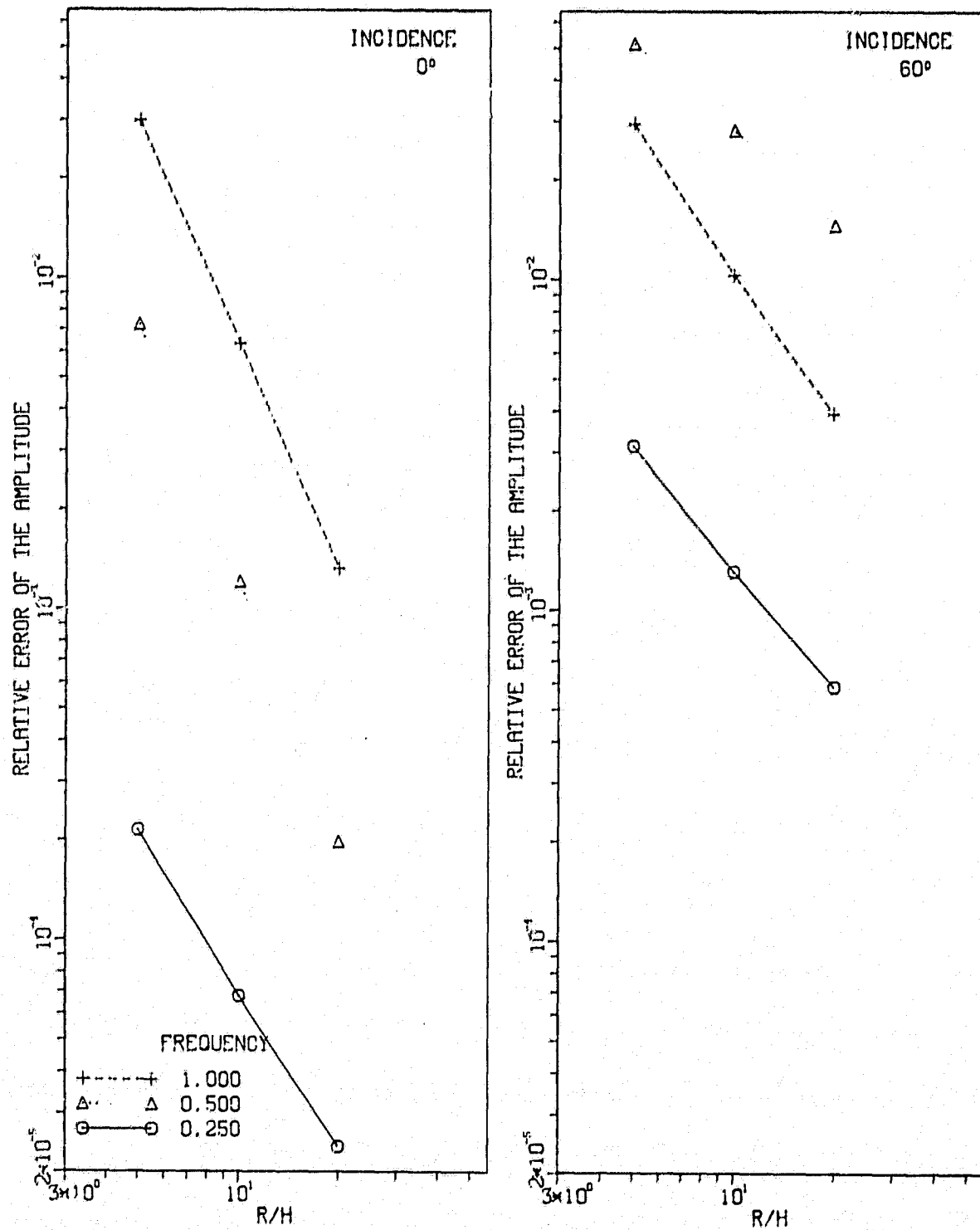


Figure 7.

RADIUS = 0.0

$P-/P+ = 1.50$

$B-/B+ = 2.00$

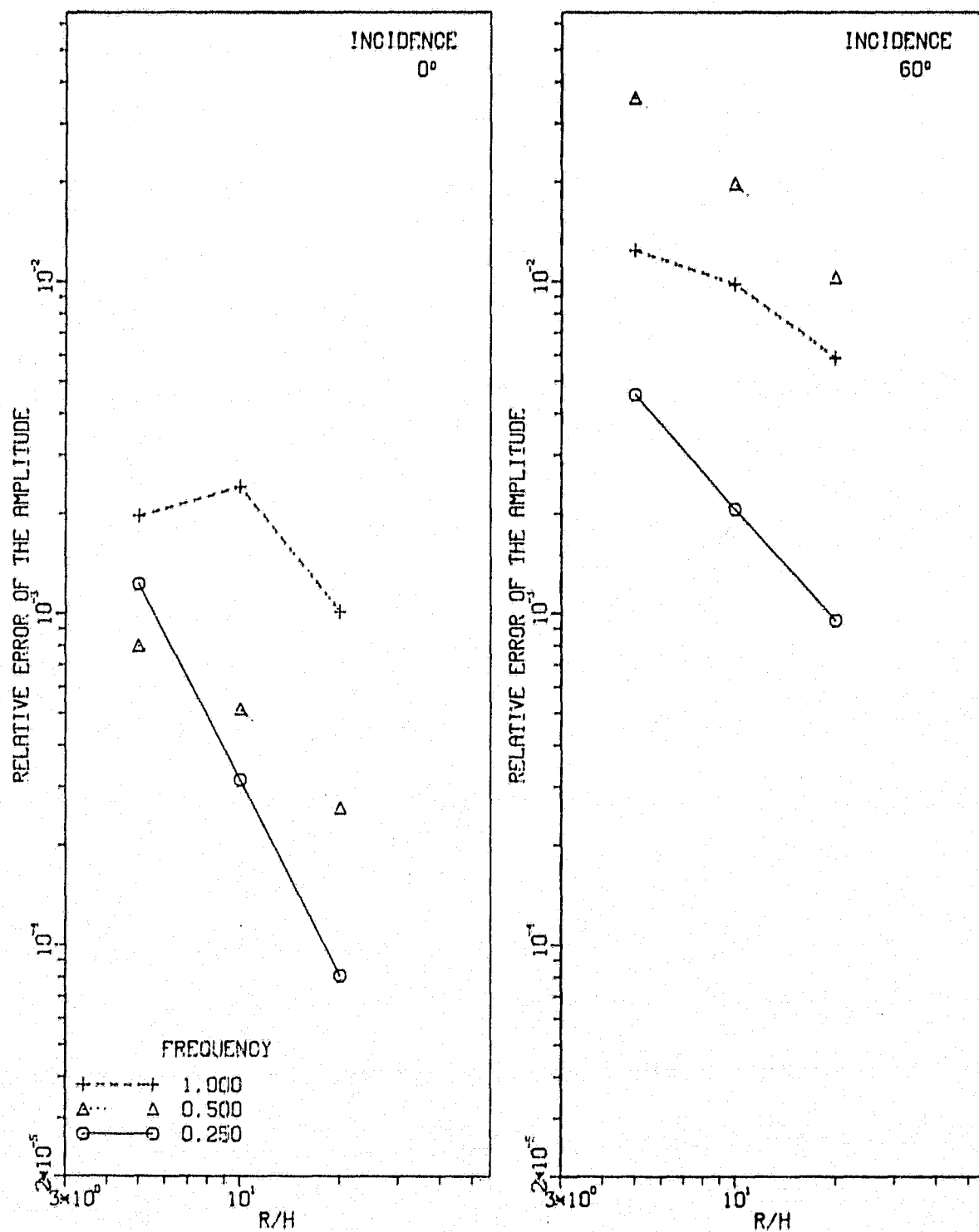


Figure 8.

RADIUS = 0.8

$P^-/P^+ = 1.50$

$B^-/B^+ = 2.00$

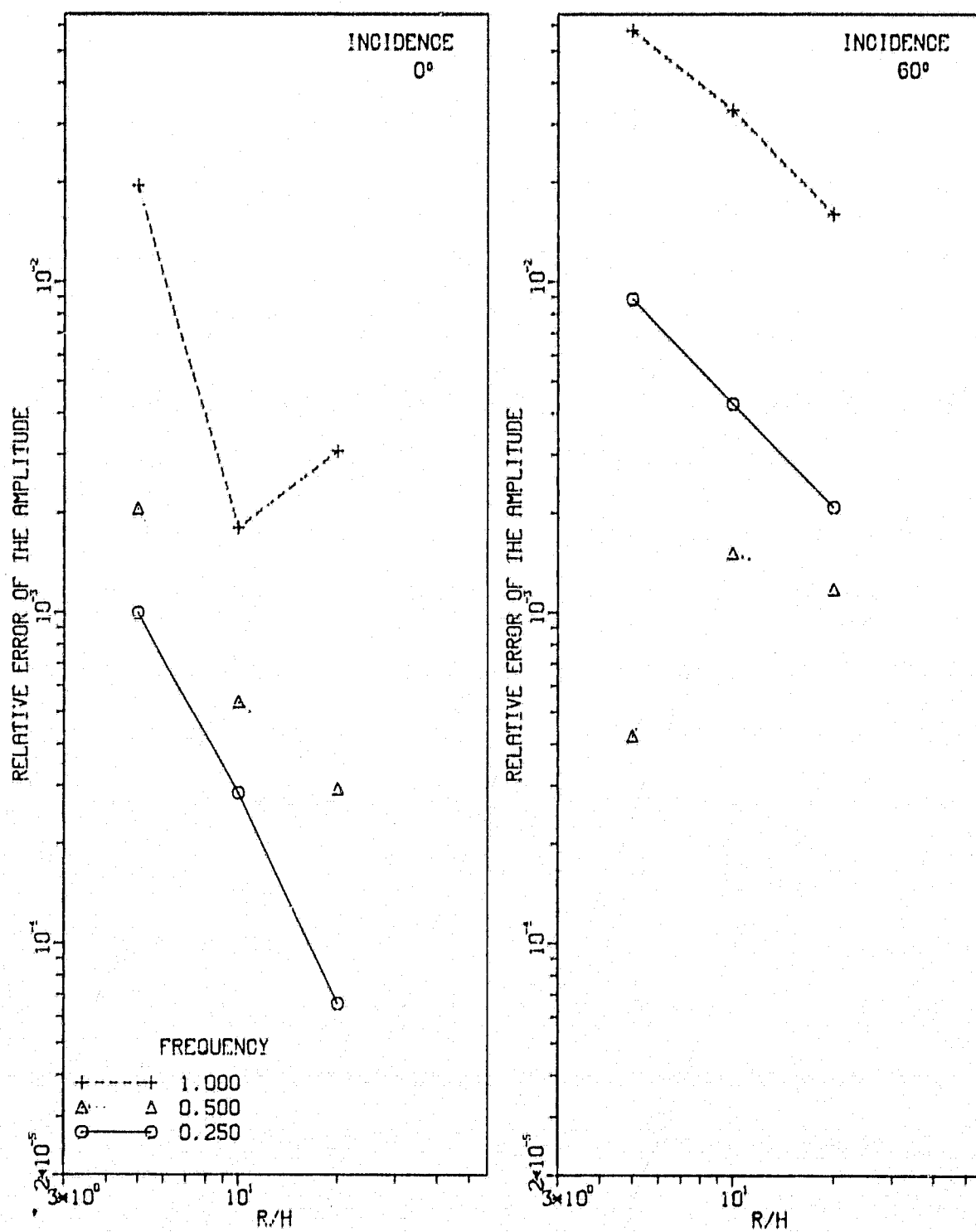


Figure 9.

TABLE 1

FREQUENCY = $.25\pi$ INCIDENCE ANGLE = 0°
 $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>
1.00	1.1717	-0.0106	1.1320	-0.0127	1.1241	-0.0129	1.1218 -0.0130
0.80	1.3671	-0.0198	1.3479	-0.0220	1.3444	-0.0222	1.3434 -0.0222
0.60	1.5405	-0.0278	1.5338	-0.0302	1.5327	-0.0304	1.5324 -0.0303
0.40	1.6787	-0.0339	1.6771	-0.0365	1.6769	-0.0367	1.6768 -0.0366
0.20	1.7713	-0.0379	1.7685	-0.0405	1.7677	-0.0407	1.7674 -0.0406
0.00	1.8209	-0.0394	1.8051	-0.0419	1.8003	-0.0421	1.7983 -0.0420

FREQUENCY = $.50\pi$ INCIDENCE ANGLE = 0°
 $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>
1.00	1.4287	-0.1334	1.2486	-0.1654	1.2172	-0.1699	1.2084 -0.1710
0.80	1.0713	0.2401	0.9829	0.2230	0.9697	0.2214	0.9661 0.2211
0.60	0.5380	0.7157	0.5122	0.7145	0.5099	0.7156	0.5094 0.7161
0.40	-0.0179	1.1896	-0.0109	1.1970	-0.0083	1.1988	-0.0074 1.1993
0.20	-0.4351	1.5505	-0.4144	1.5520	-0.4105	1.5509	-0.4094 1.5503
0.00	-0.5755	1.7429	-0.5650	1.7012	-0.5619	1.6856	-0.5605 1.6785

FREQUENCY = $.25\pi$ INCIDENCE ANGLE = 60°
 $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>
1.00	0.4901	0.9179	0.4675	0.9666	0.4386	0.9894	0.4010 1.0249
0.80	0.8362	0.8943	0.8087	0.9093	0.7939	0.9137	0.7802 0.9179
0.60	1.1733	0.7559	1.1533	0.7486	1.1436	0.7454	1.1336 0.7437
0.40	1.4662	0.5419	1.4500	0.5268	1.4424	0.5202	1.4352 0.5143
0.20	1.6883	0.2828	1.6732	0.2647	1.6672	0.2553	1.6623 0.2450
0.00	1.8274	0.0057	1.8087	-0.0171	1.8021	-0.0293	1.7983 -0.042
-0.20	1.8405	-0.2720	1.8345	-0.2982	1.8331	-0.3128	1.8328 -0.3272
-0.40	1.7617	-0.5325	1.7614	-0.5586	1.7622	-0.5743	1.7635 -0.5915
-0.60	1.5915	-0.7488	1.5923	-0.7778	1.5939	-0.7943	1.5959 -0.8129
-0.80	1.3473	-0.8902	1.3435	-0.9350	1.3422	-0.9557	1.3428 -0.9766
-1.00	1.0580	-0.9172	1.0600	-0.9884	1.0455	-1.0233	1.0237 -1.0714

FREQUENCY = $.50\pi$ INCIDENCE ANGLE = 60°
 $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>
1.00	-0.8350	0.2944	-0.8821	0.2526	-0.9628	0.2343	-1.0670 0.2269
0.80	-1.4689	1.4214	-1.5942	1.3720	-1.6468	1.3506	-1.6858 1.3345
0.60	-1.7754	2.2891	-1.8995	2.2567	-1.9418	2.2458	-1.9703 2.2405
0.40	-1.6925	2.6565	-1.7884	2.6518	-1.8177	2.6551	-1.8326 2.6631
0.20	-1.2614	2.4187	-1.3040	2.4297	-1.3125	2.4424	-1.3115 2.4603
0.00	-0.6277	1.6562	-0.5936	1.6530	-0.5765	1.6609	-0.5605 1.6785
-0.20	0.1049	0.4709	0.1593	0.5012	0.1824	0.5196	0.2013 0.5401
-0.40	0.6459	-0.6739	0.7182	-0.6506	0.7436	-0.6387	0.7595 -0.6270
-0.60	0.8930	-1.4961	0.9498	-1.4930	0.9670	-1.4922	0.9724 -1.4935
-0.80	0.8273	-1.7845	0.8337	-1.8073	0.8253	-1.8183	0.8131 -1.8324
-1.00	0.5360	-1.4826	0.5303	-1.5278	0.4653	-1.5522	0.3734 -1.5880

TABLE 2

FREQUENCY = $.25\pi$ INCIDENCE ANGLE = 0°
 $\rho_-/\rho_+ = 1.50$ $\beta_-/\beta_+ = 2.00$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.8880	0.1357	0.8863	0.1339	0.8858	0.1336	0.8856	0.1336
0.80	0.8840	0.1380	0.8837	0.1361	0.8835	0.1358	0.8835	0.1358
0.60	0.8816	0.1397	0.8819	0.1378	0.8819	0.1375	0.8819	0.1375
0.40	0.8803	0.1410	0.8807	0.1391	0.8808	0.1388	0.8808	0.1388
0.20	0.8799	0.1418	0.8801	0.1398	0.8802	0.1395	0.8803	0.1395
0.00	0.8807	0.1421	0.8802	0.1401	0.8800	0.1398	0.8800	0.1398

FREQUENCY = $.50\pi$ INCIDENCE ANGLE = 0°
 $\rho_-/\rho_+ = 1.50$ $\beta_-/\beta_+ = 2.00$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.5750	-0.0041	0.5729	-0.0052	0.5714	-0.0052	0.5706	-0.0051
0.80	0.5549	0.0065	0.5564	0.0046	0.5563	0.0044	0.5561	0.0044
0.60	0.5421	0.0148	0.5451	0.0124	0.5456	0.0121	0.5456	0.0120
0.40	0.5346	0.0206	0.5379	0.0181	0.5385	0.0177	0.5386	0.0176
0.20	0.5313	0.0240	0.5341	0.0215	0.5345	0.0211	0.5346	0.0210
0.00	0.5327	0.0249	0.5335	0.0225	0.5334	0.0222	0.5333	0.0222

FREQUENCY = $.25\pi$ INCIDENCE ANGLE = 60°
 $\rho_-/\rho_+ = 1.50$ $\beta_-/\beta_+ = 2.00$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.8750	0.3010	0.8728	0.2936	0.8711	0.2907	0.8683	0.2894
0.80	0.8828	0.2775	0.8809	0.2694	0.8800	0.2652	0.8793	0.2610
0.60	0.8876	0.2510	0.8866	0.2418	0.8862	0.2368	0.8860	0.2315
0.40	0.8888	0.2228	0.8884	0.2127	0.8883	0.2073	0.8883	0.2016
0.20	0.8861	0.1936	0.8861	0.1828	0.8861	0.1770	0.8862	0.1637
0.00	0.8798	0.1644	0.8797	0.1525	0.8798	0.1461	0.8800	0.1398
-0.20	0.8691	0.1346	0.8690	0.1217	0.8691	0.1149	0.8693	0.1155
-0.40	0.8543	0.1039	0.8542	0.0905	0.8544	0.0833	0.8545	0.0763
-0.60	0.8357	0.0733	0.8355	0.0593	0.8355	0.0517	0.8355	0.0445
-0.80	0.8136	0.0436	0.8131	0.0286	0.8127	0.0205	0.8123	0.0122
-1.00	0.7889	0.0159	0.7885	0.0006	0.7875	-0.0087	0.7852	-0.0197

FREQUENCY = $.50\pi$ INCIDENCE ANGLE = 60°
 $\rho_-/\rho_+ = 1.50$ $\beta_-/\beta_+ = 2.00$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.5944	0.2505	0.5941	0.2412	0.5930	0.2374	0.5883	0.2345
0.80	0.5973	0.2141	0.5991	0.2052	0.6009	0.2006	0.6032	0.1960
0.60	0.5914	0.1740	0.5969	0.1648	0.6006	0.1597	0.6047	0.1544
0.40	0.5753	0.1318	0.5834	0.1221	0.5881	0.1167	0.5932	0.1114
0.20	0.5486	0.0886	0.5582	0.0784	0.5635	0.0726	0.5692	0.0676
0.00	0.5126	0.0462	0.5221	0.0347	0.5275	0.0285	0.5333	0.0222
-0.20	0.4659	0.0038	0.4751	-0.0085	0.4805	-0.0150	0.4862	-0.0225
-0.40	0.4095	-0.0380	0.4183	-0.0505	0.4234	-0.0571	0.4288	-0.0641
-0.60	0.3450	-0.0777	0.3528	-0.0901	0.3573	-0.0968	0.3619	-0.1035
-0.80	0.2744	-0.1140	0.2803	-0.1264	0.2834	-0.1332	0.2865	-0.1403
-1.00	0.2006	-0.1454	0.2063	-0.1572	0.2071	-0.1645	0.2035	-0.1728

TABLE 3

FREQUENCY = 1.00π INCIDENCE ANGLE = 0°
 $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	2.6999	0.4648	1.5254	-0.0488	1.4244	-0.0224	1.4034	-0.0037
0.80	1.6630	0.9319	1.1053	0.4798	1.1905	0.5251	1.2366	0.5571
0.60	-0.1468	1.0585	-0.1258	0.7668	0.0042	0.7883	0.0607	0.8082
0.40	-1.4253	0.6158	-1.2088	0.4260	-1.1236	0.4102	-1.0900	0.4099
0.20	-1.8934	-0.1374	-1.6905	-0.2832	-1.6331	-0.3128	-1.6127	-0.3216
0.00	-2.3700	-0.5224	-1.8809	-0.6694	-1.7531	-0.6850	-1.7050	-0.6859

FREQUENCY = 1.00π INCIDENCE ANGLE = 60°
 $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	-1.1846	0.8262	-0.5685	0.4656	-0.6292	0.3569	-0.6971	0.1962
0.80	0.2819	0.5360	0.6327	0.5367	0.6107	0.6343	0.6021	0.7031
0.60	0.8912	-0.4740	0.9871	-0.3300	0.9713	-0.2135	0.9546	-0.1176
0.40	-0.3372	-1.4100	-0.3591	-1.5494	-0.3842	-1.5829	-0.4230	-1.5687
0.20	-2.1465	-1.4241	-1.9791	-1.7901	-1.9613	-1.9122	-1.9885	-1.9634
0.00	-2.3429	-0.4825	-1.8655	-0.6399	-1.7454	-0.6691	-1.7050	-0.6859
-0.20	-0.1101	0.6409	0.1856	0.8438	0.2620	0.9304	0.3148	0.9629
-0.40	1.9918	0.7143	1.8290	1.1634	1.7830	1.2555	1.7968	1.2719
-0.60	2.0383	-0.0450	1.3603	0.2858	1.1410	0.2157	1.0631	0.1366
-0.80	0.0976	-0.8284	-0.5279	-0.6316	-0.7781	-0.7939	-0.8945	-0.9124
-1.00	-1.7652	-0.9353	-1.4090	-0.7225	-1.5759	-0.7304	-1.6672	-0.6452

FREQUENCY = 1.00π INCIDENCE ANGLE = 0°
 $\rho_-/\rho_+ = 1.50$ $\beta_-/\beta_+ = 2.00$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.2325	-0.3428	0.2463	-0.3417	0.2431	-0.3396	0.2340	-0.3387
0.80	0.1802	-0.3015	0.1897	-0.3047	0.1908	-0.3045	0.1890	-0.3044
0.60	0.1525	-0.2679	0.1596	-0.2729	0.1612	-0.2736	0.1614	-0.2738
0.40	0.1390	-0.2440	0.1445	-0.2486	0.1458	-0.2496	0.1461	-0.2498
0.20	0.1333	-0.2307	0.1379	-0.2338	0.1387	-0.2344	0.1389	-0.2345
0.00	0.1343	-0.2314	0.1367	-0.2301	0.1369	-0.2295	0.1368	-0.2293

FREQUENCY = 1.00π INCIDENCE ANGLE = 60°
 $\rho_-/\rho_+ = 1.50$ $\beta_-/\beta_+ = 2.00$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.5797	0.0607	0.5966	0.0309	0.6050	0.0153	0.6036	-0.0107
0.80	0.5697	-0.0346	0.5835	-0.0500	0.5929	-0.0604	0.6013	-0.0729
0.60	0.5107	-0.1136	0.5260	-0.1194	0.5352	-0.1257	0.5448	-0.1340
0.40	0.4107	-0.1735	0.4253	-0.1752	0.4333	-0.1789	0.4416	-0.1843
0.20	0.2794	-0.2126	0.2902	-0.2126	0.2959	-0.2143	0.3016	-0.2172
0.00	0.1292	-0.2299	0.1324	-0.2288	0.1345	-0.2288	0.1368	-0.2293
-0.20	-0.0319	-0.2252	-0.0368	-0.2225	-0.0387	-0.2210	-0.0401	-0.2192
-0.40	-0.1937	-0.1995	-0.2058	-0.1951	-0.2115	-0.1917	-0.2167	-0.1874
-0.60	-0.3441	-0.1555	-0.3634	-0.1478	-0.3726	-0.1424	-0.3819	-0.1355
-0.80	-0.4743	-0.0975	-0.4994	-0.0835	-0.5119	-0.0751	-0.5265	-0.0646
-1.00	-0.5787	-0.0319	-0.6017	-0.0096	-0.6170	0.0017	-0.6438	0.0248

TABLE 4

FREQUENCY = $.7639\pi$ INCIDENCE ANGLE = 0° $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	1.2885	0.7557	0.6008	0.5329	0.4699	0.4502	0.4322	0.4191
0.80	1.7459	2.1061	0.8836	2.2977	0.6170	2.2960	0.5240	2.2857
0.60	1.5807	2.6912	0.7885	3.1921	0.4843	3.2716	0.3731	3.2874
0.40	0.8648	2.4518	0.3467	2.9921	0.1232	3.1032	0.0393	3.1337
0.20	0.0481	1.8992	-0.1567	2.2912	-0.2559	2.3843	-0.2947	2.4139
0.00	-0.2416	1.9265	-0.3773	2.0175	-0.4188	2.0315	-0.4336	2.0327

FREQUENCY = $.7639\pi$ INCIDENCE ANGLE = 60° $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.1824	-0.0520	0.5011	-0.1965	0.5007	-0.2320	0.4419	-0.3117
0.80	-0.7646	-1.7509	-0.2770	-2.1918	-0.0889	-2.3035	0.0121	-2.3884
0.60	-1.5071	-2.4883	-1.0001	-2.9706	-0.7766	-3.1009	-0.6631	-3.1864
0.40	-1.6157	-1.7282	-1.3282	-1.9749	-1.1970	-2.0368	-1.1350	-2.0708
0.20	-1.0528	0.0848	-1.0578	0.1435	-1.0509	0.1761	-1.0525	0.2039
0.00	-0.2289	1.8186	-0.3652	1.9493	-0.4119	1.9956	-0.4336	2.0327
-0.20	0.4553	2.2009	0.3285	2.1436	0.3190	2.1440	0.3292	2.1542
-0.40	0.4445	1.1071	0.5636	0.7313	0.6704	0.6352	0.7445	0.5848
-0.60	-0.0427	-0.6358	0.2801	-1.1881	0.4672	-1.3377	0.5750	-1.4226
-0.80	-0.5517	-1.8617	-0.2191	-2.2071	-0.0723	-2.2967	0.0011	-2.3533
-1.00	-0.6603	-1.8214	-0.4074	-1.6962	-0.4329	-1.6356	-0.5248	-1.5736

FREQUENCY = $.7480\pi$ INCIDENCE ANGLE = 0° $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	1.4014	0.7395	0.7765	0.6111	0.6452	0.5666	0.6046	0.5495
0.80	1.8842	1.8155	1.2719	2.0665	1.0756	2.1275	1.0040	2.1448
0.60	1.6919	2.2815	1.2144	2.7801	1.0143	2.9148	0.9374	2.9573
0.40	0.9262	2.1212	0.6445	2.6158	0.5058	2.7528	0.4511	2.7974
0.20	0.0697	1.7310	-0.0322	2.0636	-0.0911	2.1530	-0.1149	2.1824
0.00	-0.2267	1.7944	-0.3242	1.8570	-0.3524	1.8639	-0.3617	1.8621

FREQUENCY = $.7480\pi$ INCIDENCE ANGLE = 60° $\rho_-/\rho_+ = .67$ $\beta_-/\beta_+ = .50$

<u>RADIUS</u>	<u>5 ELEMENTS</u>		<u>10 ELEMENTS</u>		<u>20 ELEMENTS</u>		<u>EXACT</u>	
1.00	0.1479	-0.0826	0.4103	-0.2591	0.4024	-0.3148	0.3392	-0.4012
0.80	-0.8543	-1.6355	-0.5289	-2.0535	-0.3988	-2.1883	-0.3282	-2.2870
0.60	-1.6098	-2.3271	-1.2809	-2.7524	-1.1303	-2.8988	-1.0544	-2.9958
0.40	-1.6969	-1.6638	-1.5085	-1.8667	-1.4222	-1.9385	-1.3828	-1.9807
0.20	-1.0934	-0.0005	-1.0945	0.0607	-1.0901	0.0850	-1.0925	0.1067
0.00	-0.2196	1.6905	-0.3166	1.7924	-0.3480	1.8299	-0.3617	1.8621
-0.20	0.5098	2.2102	0.3617	2.1399	0.3431	2.1275	0.3491	2.1296
-0.40	0.5258	1.3568	0.5114	0.9991	0.5652	0.8854	0.6136	0.8226
-0.60	0.0252	-0.2368	0.1475	-0.7638	0.2579	-0.9382	0.3291	-1.0405
-0.80	-0.5396	-1.5412	-0.3682	-1.9033	-0.2769	-2.0252	-0.2283	-2.1019
-1.00	-0.7173	-1.7779	-0.5017	-1.7239	-0.5288	-1.6946	-0.6191	-1.6529

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APPENDIX A

Substituting the shape functions [equation (23)] into equation (22) is done after grouping certain terms.

1st Term

$$\begin{aligned}
 & - \int_{\Omega} \{ \mu^- (w_{x_1} \delta w_{x_1} + w_{x_2} \delta w_{x_2}) - \omega^2 \rho^- w \delta w \} d\mathbf{x} \\
 & = - \int_{\Omega} \left\{ \{\delta w\}^T [N_{x_1}] \mu^- [N_{x_1}]^T \{w\} + \{\delta w\}^T [N_{x_2}] \mu^- [N_{x_2}]^T \{w\} \right. \\
 & \quad \left. - \omega^2 \{\delta w\}^T [N] \rho^- [N]^T \{w\} \right\} d\mathbf{x}
 \end{aligned}$$

$$\text{Let } [K] = - \int_{\Omega} \{ [N_{x_1}] \mu^- [N_{x_1}]^T + [N_{x_2}] \mu^- [N_{x_2}]^T - \omega^2 [N]^T \rho^- [N] \} d\mathbf{x}$$

then the 1st term becomes

$$\{\delta w\}^T [K] \{w\} .$$

2nd Term

$$1/2 \int_{\Gamma} w^-(\mathbf{x}) \delta \mu^- w_n^-(\mathbf{x}) dS = 1/2 \int_{\Gamma} \{\delta \lambda\}^T [Q] [N_{\Gamma}]^T \{w_{\Gamma}\} dS$$

$$\text{Let } [A] = 1/2 \int_{\Gamma} [Q] [N_{\Gamma}]^T dS$$

then the 2nd term becomes

$$\{\delta \lambda\}^T [A] \{w_{\Gamma}\} .$$

3rd Term

$$\begin{aligned}
 & 1/2 \int_{\Gamma} \left\{ 1/2 \mu^+ w^-(\underline{x}) + \mu^+ \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} w^-(\underline{y}) dS_{\underline{y}} \right\} \delta \phi(\underline{x}) dS \\
 &= 1/2 \int_{\Gamma} \left\{ 1/2 \mu^+ \{\delta \phi\}^T [Q] [N_{\Gamma}]^T \{w_{\Gamma}\} dS \right. \\
 &\quad \left. + \mu^+ \int_{\Gamma} \{\delta \phi\}^T [Q] \frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} [N_{\Gamma}]^T \{w_{\Gamma}\} dS_{\underline{y}} \right\} dS
 \end{aligned}$$

$$\text{Let } [B] = 1/2 \mu^+ \left\{ 1/2 \int_{\Gamma} [Q] [N_{\Gamma}]^T dS + \int_{\Gamma} \int_{\Gamma} [Q] \left[\frac{\partial G(\underline{x}, \underline{y})}{\partial n_{\underline{y}}} \right] [N_{\Gamma}]^T dS_{\underline{y}} dS \right\}$$

then the 3rd term becomes

$$\{\delta \phi\}^T [B] \{w_{\Gamma}\} .$$

4th Term

$$\begin{aligned}
 & - 1/2 \int_{\Gamma} \int_{\Gamma} G(\underline{x}, \underline{y}) \mu^- w_n^-(\underline{y}) \delta \phi dS_{\underline{y}} dS \\
 &= 1/2 \int_{\Gamma} \int_{\Gamma} \{\delta \phi\} [Q] [G(\underline{x}, \underline{y})] [Q]^T \{\lambda\} dS_{\underline{y}} dS
 \end{aligned}$$

$$\text{Let } [C] = - 1/2 \int_{\Gamma} \int_{\Gamma} [Q] [G(\underline{x}, \underline{y})] [Q]^T dS_{\underline{y}} dS$$

then the 4th term becomes

$$\{\delta \phi\} [C] \{\lambda\} .$$

5th Term

$$\begin{aligned}
 \int_{\Gamma} \mu^- w_n^- \delta w dS - 1/2 \int_{\Gamma} \mu^- w_n^- \delta w^- dS &= \int_{\Gamma} \{\delta w_{\Gamma}\}^T [N_{\Gamma}] [Q]^T \{\lambda\} dS \\
 &- 1/2 \int_{\Gamma} \{\delta w_{\Gamma}\}^T [N_{\Gamma}] [Q]^T \{\lambda\} dS
 \end{aligned}$$

Let $[A]^T = 1/2 \int_{\Gamma} [N_{\Gamma}] [Q]^T dS$

then the 5th term becomes

$$\{\delta w_{\Gamma}\}^T [A]^T \{\lambda\} .$$

6th Term

$$\begin{aligned} & 1/2 \int_{\Gamma} \left\{ 1/2 \mu^+ \phi(\underline{x}) + \mu^+ \int_{\Gamma} \frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{x}} \phi(\underline{y}) dS_{\underline{y}} \right\} \delta w^- dS \\ &= 1/2 \int_{\Gamma} \left\{ 1/2 \mu^+ \{\delta w_{\Gamma}\}^+ [N_{\Gamma}] [Q]^T \{\phi\} \right. \\ & \quad \left. + \mu^+ \int_{\Gamma} \{\delta w_{\Gamma}\}^T [N_{\Gamma}] \left[\frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{x}} \right] [Q]^T \{\phi\} dS_{\underline{y}} \right\} dS \end{aligned}$$

Let $[B]^T = 1/2 \mu^+ \left\{ 1/2 \int_{\Gamma} [N_{\Gamma}] [Q]^T dS + \int_{\Gamma} [N_{\Gamma}] \left[\frac{\partial G(\underline{x}, \underline{y})}{\partial n \underline{x}} \right] [Q]^T dS_{\underline{y}} dS \right\}$

then the 6th term becomes

$$\{\delta w_{\Gamma}\}^T [B]^T \{\phi\} .$$

7th Term

$$\begin{aligned} & - 1/2 \int_{\Gamma} \int_{\Gamma} G(\underline{x}, \underline{y}) \phi(\underline{y}) \delta \mu^- w_n^-(\underline{x}) dS_{\underline{y}} dS \\ &= - 1/2 \int_{\Gamma} \int_{\Gamma} \{\delta \lambda\}^T [Q] [G(\underline{x}, \underline{y})] [Q]^T \{\phi\} dS_{\underline{y}} dS \end{aligned}$$

Let $[C]^T = - 1/2 \int_{\Gamma} \int_{\Gamma} [Q] [G(\underline{x}, \underline{y})] [Q]^T dS_{\underline{y}} dS$

then the 4th term becomes

$$\{\delta \lambda\}^T [C]^T \{\phi\} .$$

8th Term

$$- 1/2 \int_{\Gamma} w^{\circ}(\underline{x}) \delta \mu^{-} w_n^{-}(\underline{x}) dS = - 1/2 \int_{\Gamma} \{\delta \lambda\}^T [Q] w^{\circ} dS$$

$$\text{Let } \{f_{\lambda}\} = 1/2 \int_{\Gamma} [Q] w^{\circ} dS$$

then the 8th term becomes

$$- \{\delta \lambda\}^T \{f_{\lambda}\} .$$

9th Term

$$1/2 \int_{\Gamma} \mu^{+} w_n^{\circ} \delta w^{-} dS = 1/2 \mu^{+} \int_{\Gamma} \{\delta w_{\Gamma}\}^T [N_{\Gamma}] w_n^{\circ} dS$$

$$\text{Let } \{f_{\Gamma}\} = - 1/2 \mu^{+} \int_{\Gamma} [N_{\Gamma}] w_n^{\circ} dS$$

then the 9th term becomes

$$- \{\delta w_{\Gamma}\}^T \{f_{\Gamma}\} .$$

10th Term

$$- 1/2 \mu^{+} \int_{\Gamma} w^{\circ} \delta \phi dS = - 1/2 \mu^{+} \int_{\Gamma} \{\delta \phi\}^T [Q] w^{\circ} dS$$

$$\text{Let } \{f_{\phi}\} = \mu^{+} 1/2 \int_{\Gamma} [Q] w^{\circ} dS$$

then the 10th term becomes

$$- \{\delta \phi\}^T \{f_{\phi}\} .$$

Equation (22) now becomes:

$$\begin{aligned} & \{\delta w\}^T ([K] \{w\}) + \{\delta w_\Gamma\}^T ([B] \{\phi\} + [A]^T \{\lambda\} - \{f_\Gamma\}) \\ & + \{\delta \lambda\}^T ([A] \{w_\Gamma\} + [C]^T \{\phi\} - \{f_\lambda\}) + \{\delta \phi\}^T ([B] \{w_\Gamma\} \\ & + [C] \{\lambda\} - \{f_\phi\}) = 0 \end{aligned}$$

For arbitrary $\{\delta w\}$, $\{\delta w_\Gamma\}$, $\{\delta \lambda\}$, and $\{\delta \phi\}$; quantities multiplying them must each be zero.

$$\begin{bmatrix} K_{\Omega\Omega} & K_{\Omega\Gamma} & 0 & 0 \\ K_{\Gamma\Omega} & K_{\Gamma\Gamma} & A^T & B^T \\ 0 & A & 0 & C^T \\ 0 & B & C & 0 \end{bmatrix} \begin{Bmatrix} w_\Omega \\ w_\Gamma \\ \lambda \\ \phi \end{Bmatrix} = \begin{Bmatrix} 0 \\ f_\Gamma \\ f_\lambda \\ f_\phi \end{Bmatrix}$$

APPENDIX B. PROGRAM LISTING

C INTRODUCTION

C -----

C

C This program solves, using finite element techniques, a soil structure
C interaction problem defined in polar coordinates. The structure is a
C semicylindrical deposit of soil at the surface of an elastic halfspace.
C The properties of this deposit can be different from those of the
C halfspace and can also represent a linear change of shear modulus with
C depth. The forcing function of this problem is an incoming antiplane
C shear wave. The computed results are the steady state antiplane
C displacements. The interior deposit is represented by finite element
C techniques while the exterior halfspace is represented at the boundary
C of the deposit by the use of Green's functions. Thus only finite
C element storage requirements are for the deposit and no additional
C finite element manipulations are necessary.

C

C PROGRAM STRUCTURE

C -----

C

C The program is structured with a main driving program with various
C levels of subroutines. A schematic of this structure is shown here.

C

LEVEL 0	LEVEL 1	LEVEL 2	LEVEL 3	LEVEL 4
-----	-----	-----	-----	-----
	--- MESH			
	--- ASSM ---	-- RECT		
		-- TRI		
		-- GAMMA		
	--- FORCE ---	-- PHILAM		
		-- BMAT		
MAIN ---		-- AMAT ----	--- NORM --	--- DERIV
			--- NORM2 --	
	--- HSPACE --	-- ATEST		
		-- CMAT ----	--- DIAG --	--- FUNC
			--- DIAG2 --	
		-- CTEST		
	--- KTEST			

C

C A description of what each subroutine does is presented at the
C beginning of that subroutine.

C

C INPUT DATA

C -----

C

C The input data for this program is contained in two data files.
C FOR24.DAT contains the Gauss integration information and should not be
C changed without a series of tests to check convergence. FOR25.DAT
C contains all the other information necessary for the operation of this
C program. The unit numbers for these files are 24 and 25 respectively.
C An example of the data contained in this file is shown here:

C

C

C AMAT _____

PRECEDING PAGE BLANK NOT FIEMED

```

C CMAT
C HSPACE      --- debug switches (subroutine names)
C MESH
C START ----- signals end of debug switches (must always be used)
C UNIFORM ----- radial division method (UNIFORM or GRADIENT)
C 5.76 0.0 0.5 0.5 1.0 1.0 0.5 ----- -frequency squared
C 10 10 ----- incidence angle (radians)
C 3.14159 1.0 1 ----- shear modulus at depth
C 1.0 1.0 1.0 1.0 1.0 ----- shear modulus at surface
C                                     density of deposit
C                                     shear modulus of halfspace
C                                     _geometric shape factor (.5)
C
C                                     -number of radial divisions
C                                     _number of angular divisions
C
C                                     -angular sweep (radians)
C                                     ----- radial range
C                                     -number of boundary elements
C                                     per angular element
C
C                                     boudary node displacements
C                                     if KTEST is to be run.

```

C In use this file would look like this:

```

C
C AMAT
C CMAT
C HSPACE
C MESH
C START
C UNIFORM
C 5.76 0.0 0.5 0.5 1.0 1.0 0.5
C 10 10
C 3.14159 1.0 1
C 1.0 1.0 1.0 1.0 1.0
C
C
C OUTPUT DATA
C -----
C All output is directed to the unit number 26.
C
C

```

C MAIN PROGRAM

```

C -----
C
C The main or driving program has four major duties. The first is to
C read in the data which must be supplied by the user. A more detailed
C description of this data is presented in the "Input Data" section. The
C second duty of this subprogram is to set the bollion values for the
C various debug and method options available in this program. The
C third duty is the definition of matrix sizes. Each matrix is defined
C here using an actual number which represents the maximum size
C allowed. This limits the size of structure whcih can be analysed.
C Using the data which is read in the actual sizes of the matrices are
C calculated. These values are then used throughout the program.
C Computed matrix sizes are passed in COMMON to all subroutines while
C the matrices themselves are passed as needed through the arguments of
C the various subroutines. An expansion of the size of structure the
C program can handle can be done

```

C from this subroutine alone since this is the only place where these
C matrices are defined using actual numbers.
C However, if the size of the individual elements used is changed then
C the subroutines ASSM, RECT, and TRI must also be changed and their
C accompanying matrices.
C The final duty of this subprogram is to control the execution of
C the entire program. This is done by calling various subroutines which
C do specific jobs such as constructing particular matrices or solving
C the equations.

C
C Declare in COMMON all variables required by more
C than one C subroutine. These variables are divided into four
C categories:
C 1. SIZE This common block contains variables which define
C array dimensions.
C 2. PROB This common block contains variables which define
C problem parameters.
C 3. MAP This common block contains variables which define
C the finite element mesh.
C 4. debug This common block contains variables which define
C which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.

C
COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1 NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1 LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
INTEGER RATIO
REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
LOGICAL GRADNT
common, /debug/ dmain,dmesh,dassm,dktest,dforce,
1 dhspac,direct,dtri,dgamma,dfilam,damat,dbmat,
1 dcmat,dnorm,ddiag,ddiaq2,dfunc,dderiv,dctest,
1 datest
logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1 direct,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1 ddiag,ddiaq2,dfunc,dderiv,dctest,datest

C
C Declare and dimension arrays necessary. Only those arrays which are
C dependent on structure size are dimensioned here. This is the only
C location where actual numbers are used for these arrays. An increase
C of structure size can be handled from here alone. Arrays which are
C dependent on element size are dimensioned in RECT, TRI, and ASSM.

C
INTEGER GEOM(400,4)
REAL PROP(400,5),K(421,45),OUTPUT(421),KOG(400,21),
1 B(400,21),KOO(400,45),XL(400,23),WG(21),WO(400),
2 EXACT(400),BMATRX(20,2)
COMPLEX FG(21),FPHI(21),C(20,20),CTEMP(20),FD(21),W(21),
1 CINVER(20,20),ATRANS(21,20),ATEMP(2,21),ATEMP2(80,40),
1 ATEMP3(80,40),D(21,21),TEMPD(21,21),WHOLE(21,21),
1 LAM(20)

C
C Declare variables required in this main program.
C

LOGICAL OK

```
INTEGER debug,METHOD
REAL    FREQ,G
```

```
C
C Define whether debug is required or not.
```

```
C
C Initialize.
```

```
C
C
C      dmain = .false.
C      dmesh = .false.
C      dassm = .false.
C      dktest = .false.
C      dforce = .false.
C      dhspac = .false.
C      dbmat = .false.
C      drect = .false.
C      dtri = .false.
C      dgamma = .false.
C      dfilam = .false.
C      damat = .false.
C      dbmat = .false.
C      dcmat = .false.
C      dnorm = .false.
C      ddiag = .false.
C      ddiag2 = .false.
C      dfunc = .false.
C      dderiv = .false.
C      dctest = .false.
C      datest = .false.
```

```
C
C Read in debugs desired.
```

```
C
C      5 read(25,7)debug
C      7 format(a5)
```

```
C
C Echo debugs desired.
```

```
C
C      write(5,8)debug
C      8 format(2X,a5)
```

```
C
C Set switches for debugs desired. 'START' indicates no more
C switches will be requested.
```

```
C
C      if(debug.eq.'MAIN')dmain = .true.
C      if(debug.eq.'MESH')dmesh = .true.
C      if(debug.eq.'ASSM')dassm = .true.
C      if(debug.eq.'KTEST')dktest = .true.
C      if(debug.eq.'FORCE')dforce = .true.
C      if(debug.eq.'HSPAC')dhspac = .true.
C      if(debug.eq.'RECT')drect = .true.
C      if(debug.eq.'TRI')dtri = .true.
C      if(debug.eq.'GAMMA')dgamma = .true.
C      if(debug.eq.'PHILA')dfilam = .true.
C      if(debug.eq.'AMAT')damat = .true.
C      if(debug.eq.'BMAT')dbmat = .true.
C      if(debug.eq.'CMAT')dcmat = .true.
C      if(debug.eq.'NORM')dnorm = .true.
C      if(debug.eq.'DIAG')ddiag = .true.
C      if(debug.eq.'DIAG2')ddiag2 = .true.
C      if(debug.eq.'FUNC')dfunc = .true.
C      if(debug.eq.'DERIV')dderiv = .true.
```

```

        if(debug.eq.'CTEST')dctest = .true.
        if(debug.eq.'ATEST')datest = .true.
        if(debug.eq.'START')goto 10
        goto 5
    10    continue
C
C Define desired radial division method. If GRADIENT is desired radial
C divisions are chosen to balance element length and width. If UNIFORM
C is requested radial divisions are equal segments.
C
C Initialize.
C
C     GRADNT = .FALSE.
C
C Read in desired method.
C
C     READ(25,11)METHOD
11    FORMAT(1A5)
C
C Echo method desired.
C
C     WRITE(5,12)METHOD
12    FORMAT(2X,1A5)
C
C Set switch.
C
C     IF(METHOD.EQ.'GRADI')GRADNT = .TRUE.
C
C Read in incident wave information and soil parameters.
C
C     READ(25,*)W2,THETA0,G,GB,RO,EXTG,ALPHA
C
C Compute frequency from input squared frequency.
C
C     FREQ = SQRT(W2)
C
C Read in desired number of angular and radial divisions.
C
C     READ(25,*)NUMANG,NUMRAD
C
C Read in angle sweep of the structure (0-?radians) and the radius
C range of the structure (0-?).
C
C     READ(25,*)SWEEP,RANGE,RATIO
C
C Calculate the rate of change of soil stiffness.
C
C     GA = (G-GB)/RANGE
C
C Calculate array dimensions and make checks for program capacity.
C
C     OK = .TRUE.
C#    IF(RATIO.GE.1.AND.RATIO.LE.5) GOTO 15
C#    WRITE(5,800)
C#    OK = .FALSE.
15    BNDELM = NUMANG/RATIO
C#    I = MOD(NUMANG,RATIO)
C#    IF(1.EQ.0.AND.BNDELM.LE.15) GOTO 16
C#    WRITE(5,150)
C#    OK = .FALSE.

```

```

16  BCOLS = RATIO + 1
C#  IF(BCOLS.LE.6) GOTO 17
C#  WRITE(5,150)
C#  OK = .FALSE.
17  AWIDE = BNDELM*2
C#  IF(AWIDE.LE.30) GOTO 18
C#  WRITE(5,150)
C#  OK = .FALSE.
18  ALENG = BNDELM*RATIO*4
C#  IF(ALENG.LE.300)GOTO 19
C#  WRITE(5,150)
C#  OK = .FALSE.
19  ATMPL = RATIO*2
C#  IF(ATMPL.LE.10)GOTO 20
C#  WRITE(5,150)
C#  OK = .FALSE.
20  NUMELM = NUMANG*NUMRAD
C#  IF(NUMELM.LE.225) GOTO 21
C#  WRITE(5,100)
C#  OK = .FALSE.
21  INTNOD = NUMANG+1
C#  IF(INTNOD.LE.16) GOTO 30
C#  WRITE(5,200)
C#  OK = .FALSE.
30  NUMNOD = (INTNOD)*NUMRAD+1
C#  IF(NUMNOD.LE.241) GOTO 40
C#  WRITE(5,300)
C#  OK = .FALSE.
40  CODIAG = NUMANG + 2
C#  IF(CODIAG.LE.17) GOTO 50
C#  WRITE(5,400)
C#  OK = .FALSE.
50  NUMEQN = NUMNOD-INTNOD
C#  IF(NUMEQN.LE.225) GOTO 60
C#  WRITE(5,500)
C#  OK = .FALSE.
60  LENGTH = NUMNOD*(NUMNOD+1)/2
C#  IF(LENGTH.LE.29161) GOTO 70
C#  WRITE(5,600)
C#  OK = .FALSE.
70  WIDTH  = 2*CODIAG+1
    SPACE  = CODIAG+1

C
C If checks for program capacity are allright continue otherwise abort
C program execution.
C
    IF(OK) GOTO 80
    WRITE(5,700)
    STOP

C
C Generate finite element mesh.
C
80  CALL MESH(PROP,GEOM)
C
C Assemble structure stiffness matrix.
C
    CALL ASSM(PROP,GEOM,K,OUTPUT)
C
C Determine applied forces.
C

```



```

      CALL FORCE(FG,FPHI)
C
C Generate matrix defining halfspace.
C
      CALL HSPACE(ATRANS,ATEMP,ATEMP2,ATEMP3,BMATRX,
1 C,CTEMP,FG,FPHI,FD,OUTPUT,CINVER,TEMPD,D)
C
C I test of K matrices is desired call KTEST subroutine.
C
      IF(DKTEST)CALL KTEST(K,WO,WG,KOG,B,KOO,XL,OUTPUT,EXACT)
C
C Solve for displacements.
C
      CALL SOLVE(K,D,FG,FD,KOG,KOO,B,WHOLE,SLTN,W,XL,OUTPUT,
1 LAM,TEMPD,CINVER,FPHI)
C
C Output computed values.
C
      CALL OUT(SLTN,W,FG,FD,B,LAM)
C
C Output information supplied to program by user.
C
      WRITE(26,1000) SWEEP,NUMANG,RANGE,NUMRAD,ALPHA,RATIO
      IF(GRADNT)WRITE(26,1500)
      IF(.NOT.GRADNT)WRITE(26,1600)
      WRITE(26,2000) W2,FREQ,THETA0,GA,GB,RO,EXTG
C
C Format statements for error messages.
C
100  FORMAT(2X,'Number of elements is more than can be handled.')
150  FORMAT(2X,'Number of boundary elements is more than
1  can be handled. Ratio must be corrected.')
200  FORMAT(2X,'Number of boundary nodes is more than can be
1  handled.')
300  FORMAT(2X,'Number of nodes is more than can be handled.')
400  FORMAT(2X,'Band width is greater than can be handled.')
500  FORMAT(2X,'Number of interior nodes is more than can be
1  handled.')
600  FORMAT(2X,'Size of structure stiffness matrix is greater than
1  can be handled.')
700  FORMAT(//,2X,'Execution aborted. Storage capacity exceeded.')
800  FORMAT(2X,'Ratio must be greater than or equal to 1 and less
1  than or equal to 5.',
1  /,2X,'Execution aborted.')
C
C Formats for output of information supplied by user.
C
1000  FORMAT(//2X,'***** INPUT INFORMATION',
1  ' *****',///,
1  2X,'MESH INFORMATION',/,2X,'-----',///,
1  2X,'SWEEP = ',F11.6,2X,'NUMBER OF ANGLE DIVISIONS = ',I5,///,
1  2X,'RANGE = ',F11.6,2X,'NUMBER OF RADIAL DIVISIONS = ',I5,///,
1  2X,6X,'SHAPE CONSTANT = ',F11.6,///,
1  2X,16X,'INTERNAL BOUNDARY ELEMENTS',/,
1  2X,6X,'RATIO OF ----- =',I5,/,
1  2X,16X,'EXTERNAL BOUNDARY ELEMENTS',//)
1500  FORMAT(2X,6X,'RADIAL DIVISIONS ARE GRADUATED',//)
1600  FORMAT(2X,6X,'RADIAL DIVISIONS ARE UNIFORM',/,29X,'-----',/)
2000  FORMAT(2X,'FREE FIELD WAVE INFORMATION',/,2X,'-----',
1  ' -----',///,

```

```

1 2X,'FREQUENCY SQUARED = ',F11.6,2X,'FREQUENCY = ',F11.6,/,
1 2X,'ANGLE OF INCIDENCE FROM DOWNWARD VERTICAL = ',F11.6,/,
1 2X,'      (+ CLOCKWISE,- COUNTERCLOCKWISE)      ',/,/,
1 2X,'MATERIAL PROPERTIES',/,2X,'-----',/,/,
1 2X,'INTERNAL SHEAR MODULUS      = ',F11.6,' Y + ',F11.6,/,
1 2X,'INTERNAL MATERIAL DENSITY = ',F11.6,/,
1 2X,'EXTERNAL SHEAR MODULUS      = ',F11.6,/)

C
C Halt program execution.
C
      STOP
      END

C*****
C
C*****
C SUBROUTINE MESH
C -----
C
C The purpose of the MESH subprogram is to generate the finite element
C mesh required with a minimum of input by the user. It will generate a
C mesh for a circular structure defined in polar coordinates.
C There are only four
C required inputs. The first is the angular sweep of the entire
C structure in radians. The second is the maximum radius of the
C structure. The two remaining inputs are simply the number of divisions
C of these two structure dimensions that are desired. MESH will generate
C two tables. The first is an incidence table for each element. The
C second is a table of element coordinates and element type. These two
C tables, GEOM and PROP are passed back to the main program as they are
C used by a number of other subroutines in defining the stiffness
C matrix.
C
      SUBROUTINE MESH (PROP,GEOM)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C      array dimensions.
C   2. PROB This common block contains variables which define
C      problem parameters.
C   3. MAP This common block contains variables which define
C      the finite element mesh.
C   4. debug This common block contains variables which define
C      which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1 NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1 LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /debug/ dmain,dmesh,dassm,dktest,dforce,
1 dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1 dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest

```

```

      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1      direct,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1      ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare and dimension arrays required in this subroutine.
C
      INTEGER GEOM(NUMELM,4)
      REAL    PROP(NUMELM,5)
C
C Declare variables required only within this subroutine.
C
      INTEGER I,J,ELM
      REAL    RAD,THETA
C
C Calculate mesh sizes.
C
      DANG = SWEEP/FLOAT(NUMANG)
      DRAD = RANGE/FLOAT(NUMRAD)
      BDANG1 = DANG*RATIO
      BDANG2 = SWEEP - (BNDELM-1)*BDANG1
C
C Iterate over structure defining element coordinates and element-node
C incidences.
C
      Iterate over number of angle divisions.
C
      DO 20 I=0,NUMANG-1
C
C          Define angle: 0 to sweep minus one angle mesh size.
C
          THETA = I*DANG
C
          Iterate over number of radius divisions.
C
          DO 10 J=0,NUMRAD-1
C
C              Label element number.
C
              ELM=I*NUMRAD+J+1
C
              Define element coordinates and types:
C
              1. if radial divisions are to be uniform or
C
              IF(GRADNT) GOTO 7
              PROP(ELM,1)=(RANGE-J*DRAD)-DRAD
              PROP(ELM,2)=RANGE-J*DRAD
              GOTO 8
C
              2. if radial divisions are to be graduated.
C
              7
              PROP(ELM,1)=((1-DANG/2.0)/(1+DANG/2.0))**(J+1)
              *RANGE
              IF (J.EQ.NUMRAD-1) PROP(ELM,1)=0.0
              PROP(ELM,2)=((1-DANG/2.0)/(1+DANG/2.0))**J
              *RANGE
              1
              8
              PROP(ELM,3)=THETA
              PROP(ELM,4)=THETA+DANG
              PROP(ELM,5)=4.0
              IF (J.EQ.NUMRAD-1) PROP(ELM,5)=3.0

```

```

C
C
C          Define element node incidences.

          GEOM(ELM,1)=(J+1)*(NUMANG+1)+I+1
          IF(J.EQ.NUMRAD-1)GEOM(ELM,1)=(NUMANG+1)*NUMRAD+1
          GEOM(ELM,2)=J*(NUMANG+1)+I+1
          GEOM(ELM,3)=GEOM(ELM,2)+1
          GEOM(ELM,4)=GEOM(ELM,1)+1
          IF(J.EQ.NUMRAD-1)GEOM(ELM,4)=0

10      CONTINUE

C
C Check to see if mesh defines a complete circle. If so impose
C constraint that coordinates and incidences along angle equal 0 and
C 2Pi are the same.
C
          IF(THETA.NE.(6.28319-DANG)) GOTO 20
          PROP(ELM,3)=PROP(1,2)
          PROP(ELM,4)=PROP(1,1)
          GEOM(ELM,3)=GEOM(1,2)
          GEOM(ELM,4)=GEOM(1,1)

20      CONTINUE
C+++++
C If debug required output coordinate and incidence information.
C
      if(.not.dmesh)return
      write(26,110)
      do 30 i=1,numelm
      write(26,100)(geom(i,j),j=1,4),(prop(i,j),j=1,5)
30      continue
100     format(2x,4(i6),2x,5(f10.3))
110     format(2x,'node1 ,node2,node3 ,node4 ',2x,' ra',8x,' rb',8x,
1      ' qa',8x,' qb')
C+++++
C
C Return to main program.
C
      RETURN
      END
C*****

C*****
C SUBROUTINE ASSM
C -----
C
C The purpose of the ASSM subprogram is to assemble the structure
C stiffness matrix. It does this by looking at each element, obtaining
C its element stiffness matrix and then placing it term by term into the
C structure stiffness matrix. ASSM calls on the two subroutines RECT
C and TRI to calculate element stiffness matrices. Once the
C structure stiffness matrix is assembled ASSM returns it and the
C back to the main program for use in other subroutines.
C Another vector passed from the main program to ASSM is the OUTPUT
C vector. There is no information passed here other than the size of the
C vector. The size of the output vector is dependent on the structure
C size and therefore dimensioned in the main program for convenience.
C ASSM will output the structure stiffness matrix if debug diagnostics
C are requested.
C
      SUBROUTINE ASSM(PROP,GEOM,K,OUTPUT)

```

```

C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C       array dimensions.
C   2. PROB This common block contains variables which define
C       problem parameters.
C   3. MAP This common block contains variables which define
C       the finite element mesh.
C   4. debug This common block contains variables which define
C       which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
1  REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
1  INTEGER RATIO
1  REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
1  LOGICAL GRADNT
COMMON /debug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
1  logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare and dimension arrays required in this subroutine.
C
INTEGER GEOM(NUMELM,4)
REAL PROP(NUMELM,5),K(NUMNOD,WIDTH),OUTPUT(NUMNOD),KELM(10)
C
C Declare variables required only in this subroutine.
C
INTEGER I,N,M,ELM,JTREF1,JTREF2,JTREF3,JTREF4,PULL,ROW,
1  COL,PUSH
C
C Initialize structure stiffness matrix to zero.
C
DO 15 I=1,NUMNOD
  DO 16 J=1,WIDTH
    K(I,J)=0.0
  16 CONTINUE
15 CONTINUE
C
C Iterate through each element calculating stiffness matrix and then
C loading into structure stiffness matrix.
C
DO 50 ELM=1,NUMELM
C+++++
C If debug required output element number.
C
      if(dassm)write(26,120)elm
120      format(2x,'element=',i4)
C+++++
C Determine element type and calculate proper element
C stiffness matrix.

```

```

C
      I=ELM
      IF (PROP(ELM,5).EQ.4.0) CALL RECT (PROP,KELM,I)
      IF (PROP(ELM,5).EQ.3.0) CALL TRI (PROP,KELM,I)
C
C      Determine structure-element node reference points.
C
      JTREF1 = GEOM(ELM,1)-1
      JTREF2 = GEOM(ELM,2)-2
      JTREF3 = GEOM(ELM,3)-3
      JTREF4 = GEOM(ELM,4)-4
C
C      Iterate through each term of element stiffness matrix and
C      position it in structure stiffness matrix. Only one term of
C      each symmetric pair is considered.
C
      DO 40 N=1,int (PROP(ELM,5))
        DO 30 M=1,int (PROP(ELM,5))
          IF (M.GT.N) GOTO 40
          PULL = M + N*(N-1)/2
          IF (N.LE.1) ROW = JTREF1 + N
          IF (N.GT.1) ROW = JTREF2 + N
          IF (N.GT.2) ROW = JTREF3 + N
          IF (N.GT.3) ROW = JTREF4 + N
          IF (M.LE.1) COL = JTREF1 + M
          IF (M.GT.1) COL = JTREF2 + M
          IF (M.GT.2) COL = JTREF3 + M
          IF (M.GT.3) COL = JTREF4 + M

          I=ROW-(1+CODIAG)
          PUSH=COL-I
          K(ROW,PUSH)=K(ROW,PUSH)+KELM(PULL)
          IF (ROW.EQ.COL) GOTO 30
          I=COL-(1+CODIAG)
          PUSH=ROW-I
          K(COL,PUSH)=K(COL,PUSH)+KELM(PULL)
30          CONTINUE
40          CONTINUE
50          CONTINUE
C
C      Multiply each stiffness term by 2 to represent half circle problem.
C
      DO 51 I=1,NUMNOD
        DO 52 J=1,WIDTH
          K(I,J)=2.0*K(I,J)
52          CONTINUE
51          CONTINUE
C+++++
C If debug required output structure stiffness matrix.
C
      if (.not.dassm) return
      write(26,130)
130  format(/,2x,'**** structure stiffness matrix ****',/,
1    2X,'          band storage mode          ')
      write(26,100) (i,i=0,width)
      do 53 i=1,numnod
        write(26,200) i,(k(i,j),j=1,width)
53    continue
100  format(/,i7,100(i8))
200  format(2x,i5,2x,100(f6.2,2x))

```

```

C+++++
C
C Return to main program.
C
      RETURN
      END
C*****
C
C*****
C SUBROUTINE RECT
C -----
C
C The purpose of this subprogram is to calculate the element stiffness
C matrix for a rectangular sector of a circle. The shape functions used
C for the representation are linear in both radius and angle. The
C details of the equations used here can be seen in the accompanying
C thesis. The inputs required are the element coordinate information,
C shear modulus and density of the structure, and the frequency of the
C incoming wave. This data is supplied through the ASSM subprogram and
C the element stiffness matrix KELM is returned.
C
      SUBROUTINE RECT (PROP, KELM, ELM)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C      array dimensions.
C   2. PROB This common block contains variables which define
C      problem parameters.
C   3. MAP This common block contains variables which define
C      the finite element mesh.
C   4. dbug This common block contains variables which define
C      which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG, NUMRAD, NUMELM, INTNOD, NUMNOD, CODIAG,
1      NUMEQN, LENGTH, WIDTH, SPACE, BNDELM, BCOLS, ALENG, AWIDE, ATMPL
      INTEGER NUMANG, NUMRAD, NUMELM, INTNOD, NUMNOD, CODIAG, NUMEQN,
1      LENGTH, WIDTH, SPACE, BNDELM, BCOLS, ALENG, AWIDE, ATMPL
      COMMON /PROB/ W2, GA, GB, RO, EXTG, ALPHA, THETAO
      REAL W2, GA, GB, RO, EXTG, ALPHA, THETAO
      COMMON /MAP/ SWEEP, RANGE, DRAD, DANG, BDANG1, BDANG2, RATIO, GRADNT
      INTEGER RATIO
      REAL SWEEP, RANGE, DRAD, DANG, BDANG1, BDANG2
      LOGICAL GRADNT
      common /dbug/ dmain, dmesh, dassm, dktest, dforce,
1      dhspac, direct, dtri, dgamma, dfilam, damat, dbmat,
1      dcmat, dnorm, ddiag, ddiag2, dfunc, dderiv, dctest, datest
      logical dmain, dmesh, dassm, dktest, dforce, dhspac,
1      direct, dtri, dgamma, dfilam, damat, dbmat, dcmat, dnorm,
1      ddiag, ddiag2, dfunc, dderiv, dctest, datest
C
C Declare and dimension arrays required in this subroutine.
C KELM, KSTIF, and KMASS are element stiffness dependent and are therefore
C dimensioned with numbers here as they would have to be changed if the
C type of element were to be changed. They are independent of the
C structure size. KELM must also be dimensioned in ASSM.
C
      REAL PROP (NUMELM, 5), KELM (10), KSTIFF (10), KMASS (10), KSTIF2 (10)

```

```

C
C Declare variables required only by this subroutine.
C
      INTEGER ELM
      REAL    RA,RB,QA,QB,DIFFQ,DIFFR,RDIFSQ,DENOM
C
C Assign simplified variable names.
C
      RA = PROP(ELM,1)
      RB = PROP(ELM,2)
      QA = PROP(ELM,3)
      QB = PROP(ELM,4)
      DIFFQ = QB-QA
      DIFFR = RB-RA
      RDIFSQ = RB**2 - RA**2
      DENOM = 6.0*DIFFQ*DIFFR**2
C$
      IF(GA.EQ.0.0)GOTO 17
C
C Calculate element stiffness properties. Equations are derived in the
C text. Stiffness is composed of a variable stiffness term, a constant
C stiffness term, and a mass term. These
C are calculated seperately and then combined later in this subroutine.
C If debug is required each term is output.
C
C-----
      KSTIF2(1) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(DIFFQ**2*COS(QA)
1              +2.0*DIFFQ*SIN(QA)-2.0*(COS(QA)-COS(QB))))
1              - ((COS(QB)-COS(QA))/(3.0*DIFFQ)*DIFFR**2)
C
      ++++++
      if(direct)write(26,141)
141  format(2x,'kstif2(1-10)')
      if(direct)write(26,*)kstif2(1)
C
      ++++++
C-----
      KSTIF2(2) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(-(DIFFQ**2)*COS(QA)
1              -2.0*DIFFQ*SIN(QA)+2.0*(COS(QA)-COS(QB))))
1              - ((COS(QB)-COS(QA))/(6.0*DIFFQ)*DIFFR**2)
C
      ++++++
      if(direct)write(26,*)kstif2(2)
C
      ++++++
C-----
      KSTIF2(3) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(DIFFQ**2*COS(QA)
1              +2.0*DIFFQ*SIN(QA)-2.0*(COS(QA)-COS(QB))))
1              - ((COS(QB)-COS(QA))/(3.0*DIFFQ)*DIFFR**2)
C
      ++++++
      if(direct)write(26,*)kstif2(3)
C
      ++++++
C-----
      KSTIF2(4) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(DIFFQ*(SIN(QA)
1              +SIN(QB))-2.0*(COS(QA)-COS(QB))))
1              + ((COS(QB)-COS(QA))/(6.0*DIFFQ)*DIFFR**2)
C
      ++++++
      if(direct)write(26,*)kstif2(4)
C
      ++++++
C-----
      KSTIF2(5) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(-DIFFQ*(SIN(QA)
1              +SIN(QB))+2.0*(COS(QA)-COS(QB))))
1              + ((COS(QB)-COS(QA))/(3.0*DIFFQ)*DIFFR**2)
C
      ++++++
      if(direct)write(26,*)kstif2(5)

```



```

C      ++++++
C-----
      KSTIF2(6) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(-(DIFFQ**2)*COS(QB)
1          +2.0*DIFFQ*SIN(QB)-2.0*(COS(QA)-COS(QB))))
1          -((COS(QB)-COS(QA))/(3.0*DIFFQ)*DIFFR**2)
C      ++++++
      if(direct)write(26,*)kstif2(6)
C      ++++++
C-----
      KSTIF2(7) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(-DIFFQ*(SIN(QA)
1          +SIN(QB))+2.0*(COS(QA)-COS(QB))))
1          +((COS(QB)-COS(QA))/(3.0*DIFFQ)*DIFFR**2)
C      ++++++
      if(direct)write(26,*)kstif2(7)
C      ++++++
C-----
      KSTIF2(8) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(DIFFQ*(SIN(QA)
1          +SIN(QB))-2.0*(COS(QA)-COS(QB))))
1          +((COS(QB)-COS(QA))/(6.0*DIFFQ)*DIFFR**2)
C      ++++++
      if(direct)write(26,*)kstif2(8)
C      ++++++
C-----
      KSTIF2(9) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(DIFFQ**2*COS(QB)
1          -2.0*DIFFQ*SIN(QB)+2.0*(COS(QA)-COS(QB))))
1          -((COS(QB)-COS(QA))/(6.0*DIFFQ)*DIFFR**2)
C      ++++++
      if(direct)write(26,*)kstif2(9)
C      ++++++
C-----
      KSTIF2(10) = ((RB**3-RA**3)/(3.0*DIFFQ*DIFFR)*(-(DIFFQ**2)*COS(QB)
1          +2.0*DIFFQ*SIN(QB)-2.0*(COS(QA)-COS(QB))))
1          -((COS(QB)-COS(QA))/(3.0*DIFFQ)*DIFFR**2)
C      ++++++
      if(direct)write(26,*)kstif2(10)
C      ++++++
C-----
17 KSTIFF(1)= (DIFFQ**2*RDIFSQ + (-9.0*RB**2+12.0*RA*RB-3.0*RA**2) +
1 6.0*RB**2*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,140)
140 format(2x,'kstiff(1-10)')
      if(direct)write(26,*)kstiff(1)
C      ++++++
C-----
      KSTIFF(2)= (- (DIFFQ**2)*RDIFSQ + 3.0*RDIFSQ -
1 6.0*RA*RB*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(2)
C      ++++++
C-----
      KSTIFF(3)= (DIFFQ**2*RDIFSQ + (3.0*RB**2-12.0*RA*RB+9.0*RA**2) +
1 6.0*RA**2*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(3)
C      ++++++
C-----
      KSTIFF(4)= (-0.5*DIFFQ**2*RDIFSQ - 3.0*RDIFSQ +
1 6.0*RA*RB*ALOG(RB/RA))/DENOM
C      ++++++

```

```

      if(direct)write(26,*)kstiff(4)
C      ++++++
C-----
      KSTIFF(5)=(0.5*DIFFQ**2*RDIFSQ + (-3.0*RB**2+12.0*RA*RB-9.0*RA**2)
1      -6.0*RA**2*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(5)
C      ++++++
C-----
      KSTIFF(6)=(DIFFQ**2*RDIFSQ + (3.0*RB**2-12.0*RA*RB+9.0*RA**2) +
1      6.0*RA**2*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(6)
C      ++++++
C-----
      KSTIFF(7)=(0.5*DIFFQ**2*RDIFSQ + (9.0*RB**2-12.0*RA*RB+3.0*RA**2)
1      - 6.0*RB**2*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(7)
C      ++++++
C-----
      KSTIFF(8)=(-0.5*DIFFQ**2*RDIFSQ - 3.0*RDIFSQ +
1      6.0*RA*RB*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(8)
C      ++++++
C-----
      KSTIFF(9)=(-(DIFFQ**2)*RDIFSQ + 3.0*RDIFSQ -
1      6.0*RB*RA*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(9)
C      ++++++
C-----
      KSTIFF(10)=(DIFFQ**2*RDIFSQ + (-9.0*RB**2+12.0*RA*RB-3.0*RA**2) +
1      6.0 *RB**2*ALOG(RB/RA))/DENOM
C      ++++++
      if(direct)write(26,*)kstiff(10)
C      ++++++
C-----
      KMASS(1)=(DIFFQ)*(RB**2+2.0*RA*RB-3.0*RA**2)/36.0
C      ++++++
      if(direct)write(26,145)
145      format(2x,'kmass(1-10)')
      if(direct)write(26,*)kmass(1)
C      ++++++
C-----
      KMASS(2)=(DIFFQ)*(RDIFSQ)/36.0
C      ++++++
      if(direct)write(26,*)kmass(2)
C      ++++++
C-----
      KMASS(3)=(DIFFQ)*(3.0*RB**2-2.0*RA*RB-RA**2)/36.0
C      ++++++
      if(direct)write(26,*)kmass(3)
C      ++++++
C-----
      KMASS(4)=(DIFFQ)*(RDIFSQ)/72.0
C      ++++++
      if(direct)write(26,*)kmass(4)
C      ++++++

```

```

C-----
      KMASS(5)=(DIFFQ)*(3.0*RB**2-2.0*RA*RB-RA**2)/72.0
C      ++++++
      if (direct) write(26,*) kmass(5)
C      ++++++
C-----
      KMASS(6)=(DIFFQ)*(3.0*RB**2-2.0*RA*RB-RA**2)/36.0
C      ++++++
      if (direct) write(26,*) kmass(6)
C      ++++++
C-----
      KMASS(7)=(DIFFQ)*(RB**2+2.0*RA*RB-3.0*RA**2)/72.0
C      ++++++
      if (direct) write(26,*) kmass(7)
C      ++++++
C-----
      KMASS(8)=(DIFFQ)*(RDIFSQ)/72.0
C      ++++++
      if (direct) write(26,*) kmass(8)
C      ++++++
C-----
      KMASS(9)=(DIFFQ)*(RDIFSQ)/36.0
C      ++++++
      if (direct) write(26,*) kmass(9)
C      ++++++
C-----
      KMASS(10)=(DIFFQ)*(RB**2+2.0*RA*RB-3.0*RA**2)/36.0
C      ++++++
      if (direct) write(26,*) kmass(10)
C      ++++++
C-----
C Combine stiffness and mass terms.
C
      KELM(1)=RO*W2*KMASS(1)-GB*KSTIFF(1)-GA*KSTIF2(1)
      KELM(2)=RO*W2*KMASS(2)-GB*KSTIFF(2)-GA*KSTIF2(2)
      KELM(3)=RO*W2*KMASS(3)-GB*KSTIFF(3)-GA*KSTIF2(3)
      KELM(4)=RO*W2*KMASS(4)-GB*KSTIFF(4)-GA*KSTIF2(4)
      KELM(5)=RO*W2*KMASS(5)-GB*KSTIFF(5)-GA*KSTIF2(5)
      KELM(6)=RO*W2*KMASS(6)-GB*KSTIFF(6)-GA*KSTIF2(6)
      KELM(7)=RO*W2*KMASS(7)-GB*KSTIFF(7)-GA*KSTIF2(7)
      KELM(8)=RO*W2*KMASS(8)-GB*KSTIFF(8)-GA*KSTIF2(8)
      KELM(9)=RO*W2*KMASS(9)-GB*KSTIFF(9)-GA*KSTIF2(9)
      KELM(10)=RO*W2*KMASS(10)-GB*KSTIFF(10)-GA*KSTIF2(10)
C
C Return to ASSM subroutine.
C
      RETURN
      END
C*****
C
C*****
C SUBROUTINE TRI
C -----
C
C The purpose of this subprogram is to calculate the element stiffness
C matrix for a triangular sector of a circle. The shape functions used
C for the representation are linear in both radius and angle. The
C details of the equations used here can be seen in the accompanying
C thesis. The inputs required are the element coordinate information,
C shear modulus and density of the structure, and the frequency of the

```

```

C incoming wave. This data is supplied through the ASSM subprogram and
C the element stiffness matrix KELM is returned.
C
      SUBROUTINE TRI (PROP,KELM,ELM)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C       array dimensions.
C   2. PROB This common block contains variables which define
C       problem parameters.
C   3. MAP This common block contains variables which define
C       the finite element mesh.
C   4. debug This common block contains variables which define
C       which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1      NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1      LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /debug/ dmain,dmesh,dassm,dktest,dforce,
1      dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1      dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1      drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1      ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare and dimension arrays required in this subroutine.
C KELM, KSTIF, and KMASS are element stiffness dependent and are therefore
C dimensioned with numbers here as they would have to be changed if the
C type of element were to be changed. They are independent of the
C structure size. KELM must also be dimensioned in ASSM.
C
      REAL PROP(NUMELM,5),KELM(10),KSTIFF(10),KMASS(10),KSTIF2(10)
C
C Declare variables required only by this subroutine.
C
      INTEGER ELM
      REAL RA,RB,QA,QB,DIFFQ
C
C Assign simplified variable names.
C
      RA = PROP(ELM,1)
      RB = PROP(ELM,2)
      QA = PROP(ELM,3)
      QB = PROP(ELM,4)
      DIFFQ = QB-QA
C$ IF(GA.EQ.0.0) GOTO 17
C
C Calculate element stiffness properties. Equations are derived in the
C text. Stiffness is composed of a variable stiffness term, a constant
C striffness term, and a mass term. These

```

C are calculated separately and then combined later in this subroutine.
 C If debug is required each term is output.

```

C
C-----
      KSTIF2(1)= RB**2/(3.0*DIFFQ)*(-(DIFFQ**2)*(COS(QB)-COS(QA)))
C
C-----
      if(dtri)write(26,151)
151  format(2x,'kstif2(1-6)')
      if(dtri)write(26,*)kstif2(1)
C
C-----
      KSTIF2(2)= RB**2/(3.0*DIFFQ)*(-(DIFFQ**2)*COS(QA)+DIFFQ*
1      (SIN(QB)-SIN(QA)))
C
C-----
      if(dtri)write(26,*)kstif2(2)
C
C-----
      KSTIF2(3)= RB**2/(3.0*DIFFQ)*((DIFFQ**2)*COS(QA)+
1      2.0*DIFFQ*SIN(QA)+1.0*(COS(QB)-COS(QA)))
C
C-----
      if(dtri)write(26,*)kstif2(3)
C
C-----
      KSTIF2(4)= RB**2/(3.0*DIFFQ)*((DIFFQ**2)*COS(QB)-DIFFQ*
1      (SIN(QB)-SIN(QA)))
C
C-----
      if(dtri)write(26,*)kstif2(4)
C
C-----
      KSTIF2(5)= RB**2/(3.0*DIFFQ)*(-(DIFFQ**2)*(SIN(QA)+SIN(QB))
1      -(COS(QB)-COS(QA)))
C
C-----
      if(dtri)write(26,*)kstif2(5)
C
C-----
      KSTIF2(6)= RB**2/(3.0*DIFFQ)*(DIFFQ**2*COS(QB)
1      +2.0*DIFFQ*SIN(QB)+(COS(QB)-COS(QA)))
C
C-----
      if(dtri)write(26,*)kstif2(6)
C
C-----
17  KSTIFF(1)= 0.5*DIFFQ
C
C-----
      if(dtri)write(26,150)
150  format(2x,'kstiff(1-6)')
      if(dtri)write(26,*)kstiff(1)
C
C-----
      KSTIFF(2)= -0.25*DIFFQ
C
C-----
      if(dtri)write(26,*)kstiff(2)
C
C-----
      KSTIFF(3)= (DIFFQ**2 + 3.0)/(6.0 * DIFFQ)
C
C-----
      if(dtri)write(26,*)kstiff(3)
C
C-----
      KSTIFF(4)= -0.25*DIFFQ
C
C-----

```

```

      if(dtri)write(26,*)kstiff(4)
C      ++++++
C-----
      KSTIFF(5)=(DIFFQ**2 - 6.0)/(12.0 * DIFFQ)
C      ++++++
      if(dtri)write(26,*)kstiff(5)
C      ++++++
C-----
      KSTIFF(6)=(DIFFQ**2 + 3.0)/(6.0 * DIFFQ)
C      ++++++
      if(dtri)write(26,*)kstiff(6)
C      ++++++
C-----
      KMASS(1)=(DIFFQ)*RB**2/12.0
C      ++++++
      if(dtri)write(26,160)
160    format(2x,'kmass(1-6)')
      if(dtri)write(26,*)kmass(1)
C      ++++++
C-----
      KMASS(2)=(DIFFQ)*RB**2/24.0
C      ++++++
      if(dtri)write(26,*)kmass(2)
C      ++++++
C-----
      KMASS(3)=(DIFFQ)*RB**2/12.0
C      ++++++
      if(dtri)write(26,*)kmass(3)
C      ++++++
C-----
      KMASS(4)=(DIFFQ)*RB**2/24.0
C      ++++++
      if(dtri)write(26,*)kmass(4)
C      ++++++
C-----
      KMASS(5)=(DIFFQ)*RB**2/24.0
C      ++++++
      if(dtri)write(26,*)kmass(5)
C      ++++++
C-----
      KMASS(6)=(DIFFQ)*RB**2/12.0
C      ++++++
      if(dtri)write(26,*)kmass(6)
C      ++++++
C-----
C Combine stiffness and mass terms.
C
      KELM(1)=RO*W2*KMASS(1)-GB*KSTIFF(1)-GA*KSTIF2(1)
      KELM(2)=RO*W2*KMASS(2)-GB*KSTIFF(2)-GA*KSTIF2(2)
      KELM(3)=RO*W2*KMASS(3)-GB*KSTIFF(3)-GA*KSTIF2(3)
      KELM(4)=RO*W2*KMASS(4)-GB*KSTIFF(4)-GA*KSTIF2(4)
      KELM(5)=RO*W2*KMASS(5)-GB*KSTIFF(5)-GA*KSTIF2(5)
      KELM(6)=RO*W2*KMASS(6)-GB*KSTIFF(6)-GA*KSTIF2(6)
C
C Return to ASSM subroutine.
C
      RETURN
      END
C*****
C

```

```

C*****
SUBROUTINE KTEST(K,WO,WG,KOG,B,KOO,XL,OUTPUT,EXACT)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C 1. SIZE This common block contains variables which define
C array dimensions.
C 2. PROB This common block contains variables which define
C problem parameters.
C 3. MAP This common block contains variables which define
C the finite element mesh.
C 4. debug This common block contains variables which define
C which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1 NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1 LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
INTEGER RATIO
REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
LOGICAL GRADNT
common /debug/ dmain,dmesh,dassm,dktest,dforce,
1 dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1 dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1 drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1 ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare and dimension arrays required by this subroutine.
C
REAL K(NUMNOD,WIDTH),WO(NUMEQN),WG(INTNOD),KOG(NUMEQN,INTNOD)
1 ,B(NUMEQN,INTNOD),KOO(NUMEQN,WIDTH),XL(NUMEQN,SPACE),
2 OUTPUT(NUMNOD),EXACT(NUMEQN)
C
C Declare variables required by this subroutine.
C
INTEGER N,M,I,J,L,PULL,P,ROW,COL,IER
C
C Read in the values of displacements at the boundary nodes. These
C values are computed from the free field motion at the boundary.
C
READ(25,*) (WG(I),I=1,INTNOD)
C
C Echo imposed boundary displacements.
C
WRITE(26,725)
DO 5 J=1,INTNOD
WRITE(26,750) J,WG(J)
5 CONTINUE
C
C Partition K(omega,gamma) from structure stiffness matrix. KOG is
C pulled term by term from K. KOG is stored in full storage mode.
C
N=0
DO 20 I=INTNOD+1,NUMNOD

```

```

      N=N+1
      DO 10 J=1,INTNOD
          KOG(N,J)=0.0
          B(N,J)=0.0
          M=I-(1+CODIAG)
          PULL=J-M
          IF(PULL.LE.0) GOTO 10
          IF(PULL.GT.WIDTH) GOTO 20
          KOG(N,J)=K(I,PULL)
          B(N,J)=K(I,PULL)*-1.0
10      CONTINUE
20      CONTINUE
C
C Partition K(omega,omega) from structure stiffness matrix. KOO is
C pulled term by term from K. KOO is stored in band storage mode rather
C than symmetric storage mode to allow the use of an IMSL solving
C routine.
C
      DO 40 I=INTNOD+1,NUMNOD
          N=I-(INTNOD+1+CODIAG)
          P=N
          IF(N.LT.0) N=0
          M=I+CODIAG
          IF(M.GT.NUMNOD) M=NUMNOD
          DO 30 J=INTNOD+1+N,M
              L=I-(1+CODIAG)
              PULL=J-L
              ROW=I-INTNOD
              COL=J-INTNOD-P
              KOO(ROW,COL)=K(I,PULL)
30      CONTINUE
40      CONTINUE
C+++++
C If debug required output K(omega,gamma) and K(omega,omega).
C
      if(.not.dktest) goto 500
      write(26,300)
300    format(//,2x,'**** k(omega,gamma) ****',/)
      do 50 i=1,numeqn
          do 60 j=1,INTNOD
              output(j)=kog(i,j)
60      continue
          write(26,100) (output(n),n=1,INTNOD)
50      continue
          write(26,310)
310    format(//,2x,'**** k(omega,omega) ****',/)
      do 70 i=1,numeqn
          do 80 j=1,width
              output(j)=koo(i,j)
80      continue
          write(26,200) (output(n),n=1,width)
70      continue
C+++++
C
C Solve equation KOO x X = B = -KOG. X, the solution is written over
C top of B. This solving is done with IMSL routine LEQT1B.
C
500    CALL LEQT1B(KOO,NUMEQN,CODIAG,CODIAG,NUMEQN,B,INTNOD,NUMEQN,0,
1      XL,IER)
      IF(IER.EQ.129)write(5,400)

```



```

400  format(2x,'error')
C+++++
C If debug required output IMSL altered KO0 and solution matrix.
C
      if(.not.dktest)goto 600
      write(26,320)
320  format(//,2x,'**** modified k(omega,omega) ****',/)
      do 75 i=1,numeqn
      do 85 j=1,width
      output(j)=koo(i,j)
85   continue
      write(26,200) (output(n),n=1,width)
75   continue
      write(26,330)
330  format(//,2x,'**** solution matrix ****')
      do 90 i=1,numeqn
      do 95 j=1,INTNOD
      output(j)=B(i,j)
95   continue
      write(26,100) (output(n),n=1,INTNOD)
90   continue
100  format(2x,111f6.2)
200  format(2x,111f6.2)
C+++++
C
C Calculate interior node displacements which equals the boundary node
C displacements times the solution matrix.
C
600  DO 110 I=1,NUMEQN
      WO(I)=0.0
      DO 120 J=1,INTNOD
      WO(I)=B(I,J)*WG(J)+WO(I)
120  CONTINUE
110  CONTINUE
C
C Iterate over nodal points solving for the real portion of the
C displacements from the incident wave equation. This provides a
C partial check on the correctness of the stiffness matrix. This check
C is only valid for a uniform mass and shear modulus equal to those of
C the exterior region. Thus the solved for solution is the free field
C motion.
C
      DO 25 I=0,NUMANG
      THETA = I * DANG
      DO 15 J=1,NUMRAD
      RAD = ((1-DANG/2.0)/(1+DANG/2.0))**J*RANGE
      IF(.NOT.GRADNT)RAD=RANGE-J*DRAD
      IF(J.EQ.NUMRAD)RAD=0.0
      N=(J-1)*INTNOD+I+1
      EXACT(N)=0.5*(COS(SQRT(W2)*RAD*SIN(THETAD+THETA0))+
1      COS(SQRT(W2)*RAD*SIN(THETA-THETA0)))
15  CONTINUE
25  CONTINUE
C
C Output finite element solution and exact solution side by side for
C comparison.
C
      IF(.NOT.DKTEST)RETURN
      WRITE(26,700)
      DO 35 I=1,NUMEQN

```

```

      J=I+INTNOD
      WRITE(26,750) J,WO(I),EXACT(I)
35    CONTINUE
700   FORMAT(//,15X,'SOLVED',15X,'EXACT')
725   FORMAT(//,10X,'IMPOSED BOUNDARY DISPLACEMENTS PER',/,
1     10X,'          FREE FIELD MOTION          ')
750   FORMAT(2X,15,3X,G15.8,6X,G15.8)

C
C Return to main program.
C
      RETURN
      END

C *****
C
C *****
      SUBROUTINE FORCE(FG,FPHI)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C       array dimensions.
C   2. PROB This common block contains variables which define
C       problem parameters.
C   3. MAP This common block contains variables which define
C       the finite element mesh.
C   4. dbug This common block contains variables which define
C       which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1          NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1          LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1          dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1          dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1          drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1          ddiag,ddiag2,dfunc,dderiv,dctest,datest

C
C Declare and dimension arrays used in this subroutine.
C
      COMPLEX FG(INTNOD),FPHI(BNDELM)
      REAL XI(50),WGT(50)

C
C Declare variable required only by this subroutine.
C
      INTEGER NUMPTS,I,ELM,J
      REAL KAPPA,KAPPAR,QA,QB,THETA
      COMPLEX FGCNST,FPCNST,FG1,FG2,FPHI1,NFG1,NFG2,NFPHI1

C
C Define required constants.
C

```

```

      KAPPA = SQRT(W2*RANGE/EXTG)
      KAPPAR = KAPPA * RANGE
      FGCNST = CMPLX(0.0,-KAPPA/4.0)
      FPCNST = CMPLX(0.25,0.0)
C ++++++
C If debug required output computed constants.
C
      if(dforce)write(26,1900) fgcnst,fpcnst
C ++++++
C
C Read in Gauss integration points for numerical integration of force
C expressions.
C
      READ(24,*) NUMPTS
      DO 30 I=1,NUMPTS/2
        READ(24,*) XI(I),WGT(I)
30    CONTINUE
C-----
C
C Compute forces at boundary nodes.
C
C Initialize forces.
C
      DO 10 I=1,INTNOD
        FG(I)=(0.0,0.0)
10    CONTINUE
C ++++++
C if(dforce)write(26,1300)
C ++++++
C
C Integrate over each element for both terms of shape function.
C Contributions to common nodes are summed.
C
      DO 20 ELM=1,NUMANG
C ++++++
C j=elm
C if(dforce.and.elm.le.1)write(26,300)elm
C ++++++
C
C Define integration limits.
C
      QA = (ELM-1)*DANG
      QB = ELM*DANG
C ++++++
C if(dforce.and.elm.le.1)write(26,400)qa,qb
C ++++++
C
C Iterate through each Gauss integration point.
C
      DO 50 I=1,NUMPTS/2
C
C Transform -1 to 1 positive integration points to qa
C to qb points.
C
      THETA = ((QB-QA)*XI(I)+(QB+QA))/2.0
C ++++++
C if(dforce.and.elm.le.1)write(26,500)theta
C ++++++
C

```

Evaluate force function at positive integration point.

```
CALL GAMMA(QA,QB,THETA,KAPPA,FG1,FG2,j)
++++
if(dforce.and.elm.le.1)write(26,700)fg1,fg2
++++
```

Transform -1 to 1 negative integration points to qa to qb points.

```
THETA = ((QA-QB)*XI(I)+(QB+QA))/2.0
++++
if(dforce.and.elm.le.1)write(26,500)theta
++++
```

Evaluate force function at negative integration point.

```
CALL GAMMA(QA,QB,THETA,KAPPA,NFG1,NFG2,j)
++++
if(dforce.and.elm.le.1)write(26,800)nfg1,nfg2
++++
```

Multiply evaluation by integration weight and function constant and sum.

```
FG(ELM)=FG(ELM)+FGCNST*WGT(I)/2.0*(FG1+NFG1)
FG(ELM+1)=FG(ELM+1)+FGCNST*WGT(I)/2.0*(FG2+NFG2)
++++
if(dforce.and.elm.le.1)j=elm+1
if(dforce.and.elm.le.1)write(26,600)elm,fg(elm),
j,fg(j)
++++
```

1

```
50 CONTINUE
20 CONTINUE
```

Compute forces over elements originating from the halfspace.

Initialize forces.

```
DO 80 I=1,BNDELM
  FPHI(I) = CMPLX(0.0,0.0)
80 CONTINUE
++++
if(dforce)write(26,1400)
++++
```

Integrate over each element.

```
DO 60 ELM=1,BNDELM
  j=elm
  if(dforce.and.elm.le.1)write(26,300)elm
  +++++
```

Define integration limits.

```

QA = (ELM-1)*BDANG1
QB = ELM*BDANG1
IF(ELM.EQ.BNDELM)QA = (ELM-1)*BDANG2
IF(ELM.EQ.BNDELM)QB = ELM*BDANG2
+++++
if(dforce.and.elm.le.1)write(26,400)qa,qb
+++++

Iterate through each Gauss integration point.

DO 70 I=1,NUMPTS/2

Transform -1 to 1 positive integration points to qa
to qb points.

      THETA = ((QB-QA)*XI(I)+(QB+QA))/2.0
      +++++
      if(dforce.and.elm.le.1)write(26,500)theta
      +++++

Evaluate force function at positive integration
point.

      CALL PHILAM(THETA,KAPPAR,FPHI1,j)
      +++++
      if(dforce.and.elm.le.1)write(26,1000)fphil
      +++++

Transform -1 to 1 negative integration points to qa
to qb points.

      THETA = ((QA-QB)*XI(I)+(QB+QA))/2.0
      +++++
      if(dforce.and.elm.le.1)write(26,500)theta
      +++++

Evaluate force function at negative integration
point.

      CALL PHILAM(THETA,KAPPAR,NFPHI1,j)
      +++++
      if(dforce.and.elm.le.1)write(26,1100)nfphil
      +++++

Multiply evaluation by integration weight and
function constant and sum.

      FPHI(ELM)=FPHI(ELM)+FPCNST*(QB-QA)*WGT(I)
      /2.0*(FPHI1+NFPHI1)
      +++++
      if(dforce.and.elm.le.1)write(26,1200)elm,
      fphi(elm)
      +++++

1      70      CONTINUE
1      60      CONTINUE
-----
C Multiply forces by 2 to represent half circle.
C
DO 65 ROW=2,INTNOD-1

```

```

        FG(ROW)=2.0*FG(ROW)
65  CONTINUE
    DO 66 ROW=1,BNDELM
        FPHI(ROW)=2.0*FPHI(ROW)
66  CONTINUE
C+++++
C If debug required output FG, FPHI
C
    if(.not.dforce)RETURN
    write(26,110) numpts
    write(26,100)
    do 40 i=1,intnod
        write(26,200)i,fg(i)
40  continue
    write(26,150)
    do 45 i=1,bndelm
        write(26,200)i,fphi(i)
45  continue
    return
C
C Debug output formats.
C
100  format(//,2x,' node',14x,'fg',/,13x,'real',12x,'imaginary',/)
110  format(//,2x,'number of gauss points = ',i5)
150  format(//,2x,' node',14x,'fphi',/,13x,'real',12x,
1    'imaginary',/)
200  format(2x,i5,2x,2g15.7)
300  format(2x,'element =',i5)
400  format(2x,'qa ='g15.7,/,2x,'qb='g15.7)
500  format(2x,'theta ='g15.7)
600  format(2x,'fg(',i1,') ='2g15.7,/,2x,'fg(',i1,') ='2g15.7)
700  format(2x,'fg1 ='2g15.7,/,2x,'fg2 ='2g15.7)
800  format(2x,'nfg1 ='2g15.7,/,2x,'nfg2 ='2g15.7)
1000 format(2x,'fphil ='2g15.7)
1100 format(2x,'nfphil ='2g15.7)
1200 format(2x,'fphi(',i1,') ='2g15.7)
1300 format(2x,'***** fg check *****')
1400 format(///,2x,'***** fphi check *****')
1900 format(2x,'fgcnst ='2g15.7,/,
1    2x,'fpcnst ='2g15.7)
    END
C*****
C
C*****
    SUBROUTINE GAMMA(QA,QB,THETA,KAPPAR,FG1,FG2,elm)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four catagories:
C 1. SIZE This common block contains variables which define
C    array dimensions.
C 2. PROB This common block contains variables which define
C    problem parameters.
C 3. MAP This common block contains variables which define
C    the finite element mesh.
C 4. dbug This common block contains variables which define
C    which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
    COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,

```

```

1      NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1      LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /dbg/ dmain,dmesh,dassm,dktest,dforce,
1      dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1      dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1      drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1      ddiag,ddiag2,dfunc,dderiv,dctest,datest

```

C
C Declare variables used only in this subroutine.
C

```

      INTEGER elm
      REAL QA,QB,THETA,KAPPAR,C,D
      DOUBLE PRECISION SINDIF,SINSUM,CSSUM,SSDIF,SSSUM,A,B
      COMPLEX FG1,FG2,FGAMAA,NGAMA1,NGAMA2

```

C
C Evaluate force function for the two terms of the shape function.
C

```

      SINDIF = SIN(THETA-THETAO)
      SINSUM = SIN(THETA+THETAO)
      CSDIF = COS(KAPPAR*SINDIF)
      CSSUM = COS(KAPPAR*SINSUM)
      SSDIF = SIN(KAPPAR*SINDIF)
      SSSUM = SIN(KAPPAR*SINSUM)
      A = SINSUM*CSSUM-SINDIF*CSDIF
      B = SINSUM*SSSUM+SINDIF*SSDIF
      C = A
      D = B
      FGAMAA = CMPLX(C,D)
      NGAMA1 = CMPLX((QB-THETA),0.0)
      NGAMA2 = CMPLX((THETA-QA),0.0)
      FG1 = NGAMA1*FGAMAA
      FG2 = NGAMA2*FGAMAA

```

C
C If debug required write results of computations.
C

```

      if(dgamma.and.elm.le.1)write(26,100)sindif,sinsum,csdif,
1      cssum,ssdif,sssum,fgamaa,ngamal,ngama2,fg1,fg2
      ++++++

```

C
C Format statements for debug output.
C

```

100  format(//,2x,'sindif =',g15.7,/,
      2x,'sinsum =',g15.7,/,
      2x,'csdif =',g15.7,/,
      2x,'cssum =',g15.7,/,
      2x,'ssdif =',g15.7,/,
      2x,'sssum =',g15.7,/,
      2x,'fgamaa =',2g15.7,/,
      2x,'ngamal =',2g15.7,/,
      2x,'ngama2 =',2g15.7,/,
      2x,'fg1 =',2g15.7,/,
      2x,'fg2 =',2g15.7,/)

```

```

C
C Return to FORCE subroutine.
C
      RETURN
      END
C*****
C
C*****
      SUBROUTINE PHILAM(THETA,KAPPAR,F1,elm)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C       array dimensions.
C   2. PROB This common block contains variables which define
C       problem parameters.
C   3. MAP This common block contains variables which define
C       the finite element mesh.
C   4. dbug This common block contains variables which define
C       which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare variables used only in this subroutine.
C
      INTEGER elm
      REAL THETA,KAPPAR,C,D
      DOUBLE PRECISION SINDIF,SINSUM,CSSUM,SSDIF,SSSUM,A,B
      COMPLEX F1
C
C Evaluate force function.
C
      SINDIF = SIN(THETA-THETAO)
      SINSUM = SIN(THETA+THETAO)
      CSDIF = COS(KAPPAR*SINDIF)
      CSSUM = COS(KAPPAR*SINSUM)
      SSDIF = SIN(KAPPAR*SINDIF)
      SSSUM = SIN(KAPPAR*SINSUM)
      A = CSSUM + CSDIF
      B = SSSUM - SSDIF
      C = A
      D = B
      F1 = CMPLX(C,D)

```



```

C *****
C If debug required output computed values.
C
      if(dfilam.and.(elm.le.1.or.elm.eq.3000))write(26,100)sindif,
1  sinsum,csdif,cssum,ssdif,sssum,f1
C *****
C
C Format statements for debug output.
C
100  format(//,2x,'sindif =',g15.7/,
          2x,'sinsum =',g15.7/,
          2x,'csdif =',g15.7/,
          2x,'cssum =',g15.7/,
          2x,'ssdif =',g15.7/,
          2x,'sssum =',g15.7/,
          2x,'f1 =',2g15.7,/)
C
C Return to FORCE subroutine.
C
      RETURN
      END
C *****
C *****
C *****
      SUBROUTINE HSPACE(ATRANS,ATEMP,ATEMP2,ATEMP3,BMATRX,
1  C,CTEMP,FG,FPHI,FD,OUTPUT,CINVER,TEMPD,D)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C 1. SIZE This common block contains variables which define
C    array dimensions.
C 2. PROB This common block contains variables which define
C    problem parameters.
C 3. MAP This common block contains variables which define
C    the finite element mesh.
C 4. debug This common block contains variables which define
C    which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /debug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare and dimension arrays used in this subroutine.
C
      REAL OUTPUT(INTNOD),BMATRX(BNDELM,BCOLS)

```

```

        COMPLEX ATEMP(ATMPL,AWIDE),CINVER(BNDELM,BNDELM),
1          TEMPD(INTNOD,INTNOD),D(INTNOD,INTNOD),
1          ATRANS(INTNOD,BNDELM),ATEMP2(ALENG,AWIDE),
1          ATEMP3(ALENG,AWIDE),FD(BNDELM),
1          C(BNDELM,BNDELM),CTEMP(NUHANG),FG(INTNOD),FPHI(BNDELM)
C
C Declare variables used only in this subroutine.
C
        INTEGER ROW,COL,I,PUSH,IER,COL1,COL2
C
C Determine B matrix.
C
        CALL BMAT(BMATRX,OUTPUT)
C
C Determine A matrix.
C
        CALL AMAT(ATRANS,ATEMP,ATEMP2,ATEMP3)
C
C If a test of the amatrix is desired run ATEST.
C
        IF(DATEST)CALL ATEST(ATRANS,FG,BMATRX)
C
C Complete A matrix by addition of term similar to B matrix.
C
C
C Iterate through rows and columns of BMATRX, modify constant and add
C to appropriate term in ATRANS.
C
        DO 110 ROW=1,BNDELM
            DO 115 COL=1,BCOLS
                PUSH=RATIO*(ROW-1)+COL
                ATRANS(PUSH,ROW)=ATRANS(PUSH,ROW) -
1                ALPHA*BMATRX(ROW,COL)
115          CONTINUE
110        CONTINUE
C
C If debug desired output ATRANS.
C
        if(.not.dhspac)goto 113
        write(26,5000)
        do 111 row=1,intnod
            write(26,1000)(atrans(row,col),col=1,bndelm)
111        continue
C
C
C Determine C matrix.
C
113        CALL CMAT(C,CTEMP)
C
C If test of C matrix is desired run CTEST.
C
        IF(DCTEST)CALL CTEST(FPHI,C)
C
C If debug desired output C matrix.
C
        if(.not.dhspac)goto 36
        write(26,2000)
        do 35 row=1,bndelm
            write(26,1000)(c(row,col),col=1,bndelm)
35        continue

```

```

C      ++++++
C
C Perform condensation of exterior matrices to one matrix
C representing the exterior at the boundary elements only.
C
C
C Store C matrix in temporary storage so it can be inverted without
C destruction.
C
  36  DO 5 ROW=1,BNDELM
        DO 10 COL=1,BNDELM
              ATEMP2(ROW,COL)=C(ROW,COL)
  10      CONTINUE
  5      CONTINUE
C
C Invert C matrix according to instructions in IMSL manual for LEQT1C.
C
      CALL LEQT1C(ATEMP2,BNDELM,ALENG,CTEMP,1,BNDELM,1,OUTPUT,IER)
      CTEMP(1) = CMPLX(1.0,0.0)
      DO 15 ROW=2,BNDELM
            CTEMP(ROW) = CMPLX(0.0,0.0)
  15      CONTINUE
      DO 20 COL=1,BNDELM
            CALL LEQT1C(ATEMP2,BNDELM,ALENG,CTEMP,1,BNDELM,2,OUTPUT,IER)
            DO 25 ROW=1,BNDELM
                  CINVER(ROW,COL) = CTEMP(ROW)
                  CTEMP(ROW) = CMPLX(0.0,0.0)
                  IF(ROW.EQ.COL+1)CTEMP(ROW) = CMPLX(1.0,0.0)
  25      CONTINUE
  20      CONTINUE
C      ++++++
C If debug required output inverse of C matrix.
C
      if(.not.dhspac)goto 31
      write(26,2500)
      do 30 row=1,bndelm
            write(26,1000)(cinver(row,col),col=1,bndelm)
  30      continue
C      ++++++
C Initialize product of C inverse transpose times B to zero.
C
  31  DO 40 ROW=1,BNDELM
        DO 45 COL=1,INTNOD
              TEMPD(ROW,COL) = CMPLX(0.0,0.0)
  45      CONTINUE
  40      CONTINUE
C
C Multiply C inverse transpose times B. Actual method is to multiply B
C transpose times C inverse and then transposing the result. This is
C done because of the way B is stored.
C
      DO 50 COL1=1,BNDELM
            DO 55 ROW=1,BNDELM
                  PUSH = RATIO*(ROW-1)
                  DO 60 COL2=1,BCOLS
                        TEMPD(COL1,PUSH+COL2)=
  1                      TEMPD(COL1,PUSH+COL2) +
  1                      BMATRX(ROW,COL2)*CINVER(ROW,COL1)
  60      CONTINUE

```

```

55      CONTINUE
50      CONTINUE
C      ++++++
C If debug desired output C inverse transpose times B.
C
      if(.not.dhspac)goto 66
      write(26,3000)
      do 65 row=1,bndelm
          write(26,1000) (tempd(row,col),col=1,intnod)
65      continue
C      ++++++
C
C Multiply A transpose times C inverse transpose times B.
C
66      DO 70 COL1=1,INTNOD
          DO 75 ROW=1,INTNOD
              ATEMP2(ROW,COL1) = CMPLX(0.0,0.0)
              DO 80 COL2=1,BNDELM
                  ATEMP2(ROW,COL1)=ATEMP2(ROW,COL1) +
1                  ATRANS(ROW,COL2)*TEMPD(COL2,COL1)
80      CONTINUE
75      CONTINUE
70      CONTINUE
C      ++++++
C If debug desired output A transpose times C inverse times B.
C
      if(.not.hspac) goto 86
      write(26,3500)
      do 85 row=1,intnod
          write(26,1000) (ATEMP2(row,col),col=1,intnod)
85      continue
C      ++++++
C
C Complete halfspace matrix D by taking negative of the sum of the
C matrix just computed and its transpose.
C
86      DO 90 ROW=1,INTNOD
          DO 95 COL=1,INTNOD
              D(ROW,COL)=-ATEMP2(ROW,COL)-ATEMP2(COL,ROW)
95      CONTINUE
90      CONTINUE
C      ++++++
C If debug desired output D matrix.
C
      if(.not.dhspac) goto 101
      write(26,4000)
      do 100 row=1,intnod
          write(26,1000) (d(row,col),col=1,intnod)
100     continue
C      ++++++
C
C Condense external force vectors to a single force vector at the
C boundary.
C
C
C Determine FD.
C
C Multiply B transpose times C inverse times FPHI.
C
101     DO 165 ROW=1,INTNOD

```

```

                FD(ROW) = CMPLX(0.0,0.0)
                DO 170 COL=1,BNDELM
                    FD(ROW) = FD(ROW)+TEMPD(COL,ROW)*FPHI(COL)
170             CONTINUE
165             CONTINUE
C$             write(26,*)(fd(row),row=1,intnod)
C
C             Multiply A transpose times C inverse transpose.
C
                DO 175 COL1=1,BNDELM
                    DO 180 ROW=1,INTNOD
                        TEMPD(ROW,COL1) = CMPLX(0.0,0.0)
                        DO 185 COL2=1,BNDELM
                            TEMPD(ROW,COL1) = TEMPD(ROW,COL1) +
                                ATRANS(ROW,COL2)*CINVER(COL1,COL2)
185             CONTINUE
180             CONTINUE
175             CONTINUE
                if(.not.dhspac) goto 177
                write(26,5500)
                do 176 row=1,intnod
                    write(26,1000)(tempd(row,col),col=1,bndelm)
176             continue
C
C             Multiply A transpose times C inverse transpose times FPHI.
C
177             DO 190 ROW=1,INTNOD
                DO 195 COL=1,BNDELM
                    FD(ROW) = FD(ROW)-TEMPD(ROW,COL)*FPHI(COL)
195             CONTINUE
190             CONTINUE
C$             write(26,*)(fd(row),row=1,intnod)
C
C             Debug format statements.
C
5500             FORMAT(/2X,'***** A TRANSPOSE TIMES C INVERSE TRANSPOSE
1             *****')
5000             FORMAT(/2X,'***** ATRANS *****')
4000             FORMAT(/2X,'***** D MATRIX *****')
3500             FORMAT(/2X,'***** ATRANS TIMES CINVER TIMES B *****')
3000             FORMAT(/2X,'***** C INVERS TRANSPOSE TIMES B *****')
2500             FORMAT(/2X,'***** C INVERSE *****')
2000             FORMAT(/2X,'***** C MATRIX *****')
1000             FORMAT(1X,100F7.4)
                return
                END
C *****
C
C *****
                SUBROUTINE BMAT(BMATRX,OUTPUT)
C
C             Declare in COMMON all variables required by more than one
C             subroutine. These variables are divided into four catagories:
C             1. SIZE This common block contains variables which define
C                 array dimensions.
C             2. PROB This common block contains variables which define
C                 problem parameters.
C             3. MAP This common block contains variables which define
C                 the finite element mesh.
C             4. debug This common block contains variables which define

```

```

C          which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATNPL
1  INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATNPL
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
COMMON /MODE/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
1  INTEGER RATIO
1  REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
1  LOGICAL GRADNT
1  common /debug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
1  logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare and dimension arrays used in this subroutine.
C
REAL BMATRX(BNDELM,BCOLS),OUTPUT(INTNOD)
C
C Declare variables used in this subroutine only.
C
INTEGER I,J,ELM,RCW,COL
REAL ANS
C
C Calculate integral from derived expression. The terms of the integral
C for both shape functions are the same.
C
ANS=0.25*DANG
C
C Position these values in the proper location of the B matrix. The
C positioning is derived from the use of a circulant matrix which is
C condensed to the one for a half-circle. Only the non-zero terms are
C stored.
C
DO 60 ROW=1,BNDELM
    BMATRX(ROW,1)=2.0*ANS
    BMATRX(ROW,BCOLS)=2.0*ANS
    IF(BCOLS.EQ.2) GOTO 60
    DO 70 COL=2,BCOLS-1
        BMATRX(ROW,COL)=2.0*ANS
    70 CONTINUE
60 CONTINUE
C *****
C If debug is desired output both the stored version of the B matrix and
C the full representation for the half-circle. Otherwise return to
C HSPACE subroutine.
C
if(.not.dbmat)RETURN
write(26,300)
do 40 i=1,bndelm
    do 50 j=1,bcols
        output(j)=BMATRX(i,j)
    50 continue
    write(26,200) (output(j),j=1,bcols)
40

```

```

40  continue
    write(26,400) (i,i=1,intnod)
    do 10 row=1,bndelm
        do 20 col=1,intnod
            output(col)=0.0
20      continue
        push = ratio*(row-1)
        do 30 col=1,ratio+1
            output(push+col)=bmatrx(row,col)
30      continue
        write(26,100) row,(output(i),i=1,intnod)
10  continue
C    ++++++
C
C Debug format statements
C
100  format(2x,i2,1x,100f11.6)
200  format(2x,10f6.3)
300  format(/2x,'***** compact b matrix *****',/)
400  format(//2x,'***** full b matrix *****',//
1    ,7x,100(i2,4x))
C
C Return to HSPACE subroutine.
C
    return
    END
C*****
C
C*****
SUBROUTINE AMAT(ATRANS,ATEMP,ATEMP2,ATEMP3)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four catagories:
C 1. SIZE This common block contains variables which define
C    array dimensions.
C 2. PROB This common block contains variables which define
C    problem parameters.
C 3. MAP This common block contains variables which define
C    the finite element mesh.
C 4. dbug This common block contains variables which define
C    which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
INTEGER RATIO
REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
LOGICAL GRADNT
common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest

```

```

C
C Declare in COMMON the Gauss integration points.
C
      COMMON /INGRAL/ NUMPTY,YVALUE,WGTY,NUMPTZ,ZVALUE,WGTZ
      INTEGER NUMPTY,NMPTYD,NUMPTZ
C
C Declare and dimension arrays required in this subroutine.
C
      COMPLEX ATEMP(2,ALENG),TEMP,
1  ATRANS(INTNOD,BNDELM),ATEMP2(ATMPL,AWIDE),ATEMP3(ALENG,AWIDE)
      REAL YVALUE(100),WGTY(100),ZVALUE(100),WGTZ(100)
C
C Declare variables used only in this subroutine.
C
      INTEGER I,ROW,COL,SOURCE,PULL1,PULL2,OBSERV,PUSH,LIMIT,
1  PULL,WOR,PUSH1,PUSH2
      REAL QAOBS,QBOBS,QASRC,QBSRC,TEST
      LOGICAL ODD
C
C Read in Gauss integration points.
C
      READ(24,*) NUMPTY
      DO 5 I=1,NUMPTY/2
        READ(24,*) YVALUE(I),WGTY(I)
5  CONTINUE
      READ(24,*) NUMPTZ
      DO 10 I=1,NUMPTZ/2
        READ(24,*) ZVALUE(I),WGTZ(I)
10 CONTINUE
C
      *****
      if(damat)write(26,7000) numptz,numpty
      *****
C
C Determine if number of interior boundary elements per exterior
C boundary element is odd or even. Set limits on the number of observer
C integrals necessary.
C
      ODD = .FALSE.
      LIMIT = RATIO/2
      TEST = RATIO - 2*LIMIT
      IF(TEST.NE.0) ODD = .TRUE.
      IF(LIMIT.EQ.0) GOTO 16
C
C Perform double integral for A matrix. Outer integrals are the
C observers.
C
C Iterate over necessary observers.
C
      DO 30 OBSERV=1,LIMIT
C
      *****
      if(damat)write(26,500) observ
      *****
C
C Determine limits of integration for observer.
C
      QAOBS = (OBSERV-1)*DANG
      QBOBS = OBSERV*DANG
C
      *****
      if(damat)write(26,600) qaoobs,qboobs

```



```

C          ++++++
C
C      Iterate over necessary sources.
C
C          DO 15 SOURCE=1,BNDELM*2
C              ++++++
C              if(damat)write(26,700) source
C              ++++++
C
C      Determine limits of integration for the source.
C
C          QASRC = (SOURCE-1)*BDANG1
C          QBSRC = SOURCE*BDANG1
C          ++++++
C          if(damat)write(26,800)qasrc,qbsrc
C          ++++++
C
C      Determine temporary storage slot for observer-source
C      integral.
C
C          PUSH = (OBSERV-1)*AWIDE+SOURCE
C
C      Evaluate integral.
C
C          IF(SOURCE.EQ.1) GOTO 11
C          CALL NORM2(QAOBS,QBOBS,QASRC,QBSRC,
1              ATEMP(1,PUSH),ATEMP(2,PUSH))
C          GOTO 12
C          CALL NORM(QAOBS,QBOBS,QASRC,QBSRC,
11             ATEMP(1,PUSH),ATEMP(2,PUSH))
C          ++++++
C          12  if(damat)write(26,900)push,atemp(1,push),push,
C              atemp(2,push)
C          15  ++++++
C          15  CONTINUE
C          30  CONTINUE
C
C      If number of internal boundary elements per external boundary element
C      is odd perform integral for the odd observer. This is done here since
C      the number of sources is less than for the other observers due to
C      symmetry.
C
C          IF(.NOT.ODD) GOTO 20
C          16  OBSERV = LIMIT+1
C
C      Determine limits of integration for observer.
C
C          QAOBS = (OBSERV-1)*DANG
C          QBOBS = OBSERV*DANG
C          ++++++
C          if(damat)write(26,600)qaobs,qbobs
C          ++++++
C
C      Iterate over necessary sources.
C
C          DO 25 SOURCE=1,BNDELM+1
C              ++++++
C              if(damat)write(26,700) source
C              ++++++
C

```

```

C      Determine limits of integration for source.
C
C          QASRC = (SOURCE-1)*BDANG1
C          QBSRC = SOURCE*BDANG1
C          ++++++
C          if(damat)write(26,800)qasrc,qbsrc
C          ++++++
C
C      Determine temporary storage slot for observer-source
C      integral.
C
C          PUSH = (OBSERV-1)*AWIDE+SOURCE
C          IF(SOURCE.EQ.1)GOTO 21
C
C      Evaluate integral.
C
C          CALL NORM2(QAOBS,QBOBS,QASRC,QBSRC,
1              ATEMP(1,PUSH),ATEMP(2,PUSH))
C          GOTO 22
C      21. CALL NORM(QAOBS,QBOBS,QASRC,QBSRC,
1              ATEMP(1,PUSH),ATEMP(2,PUSH))
C          ++++++
C      22. if(damat)write(26,900)push,atemp(1,push),push,
1              atemp(2,push)
C          ++++++
C      25      CONTINUE
C
C          ++++++
C      If debug desired output computed integrals.
C
C      20  if(.not.damat) goto 36
C          write(26,300)
C          limit=ratio*bndelm
C          if(odd)limit=limit+1
C          do 35 col=1,limit
C              write(26,400)(atemp(row,col),row=1,2)
C      35  continue
C          ++++++
C
C      Determine if number of interior boundary elements per exterior
C      boundary element is odd or even. Set limits on the length of A
C      matrix and test value.
C
C      36  LIMIT = RATIO/2
C          IF(ODD) LIMIT = LIMIT+1
C          TEST = RATIO*BNDELM
C          IF(ODD) TEST=TEST+1
C
C-----
C      CREATE UNIT MATRIX
C          DO 50 ROW=1,LIMIT
C              PUSH = ROW*2
C              DO 40 COL=1,BNDELM*2
C                  PULL=(ROW-1)*BNDELM*2+COL
C                  IF(PULL.GT.TEST) GOTO 37
C                  ATEMP2(PUSH-1,COL)=ATEMP(1,PULL)
C                  ATEMP2(PUSH,COL)=ATEMP(2,PULL)
C                  GOTO 40
C      37  PULL = 2*TEST-PULL
C          ATEMP2(PUSH-1,COL)=ATEMP(2,PULL)
C          ATEMP2(PUSH,COL)=ATEMP(1,PULL)

```

```

40      CONTINUE
      IF(ROW.EQ.LIMIT.AND.ODD)GOTO 50
      WOR = RATIO+1-ROW
      PUSH = WOR*2
      DO 45 COL=1,BNDELM*2
          PULL=2+ROW*BNDELM*2-COL
          IF(PULL.GT.ROW*BNDELM*2)PULL=PULL-BNDELM*2
          ATEMP2(PUSH-1,COL)=ATEMP(1,PULL)
          ATEMP2(PUSH,COL)=ATEMP(2,PULL)

45      CONTINUE
50      CONTINUE
      if(.not.damat) goto 56
      write(26,2000)
      do 55 row=1,ratio*2
          write(26,7600) (atemp2(row,col),col=1,bndelm*2)
55      continue
C SETUP BIG A MATRIX
56      DO 70 I=1,BNDELM*2
          DO 65 ROW=1,RATIO*2
              PUSH1 = ROW+(I-1)*RATIO*2
              DO 60 COL=1,BNDELM*2
                  PUSH2 = COL+I-1
                  IF(PUSH2.GT.BNDELM*2)PUSH2 =
1                  PUSH2-2*BNDELM
                  ATEMP3(PUSH1,PUSH2)=ATEMP2(ROW,COL)
60          CONTINUE
65      CONTINUE
70      CONTINUE
      if(.not.damat)goto 72
      write(26,7100)
      do 71 row=1,bndelm*ratio*4
          write(26,7600) (atemp3(row,col),col=1,bndelm*2)
71      continue
C ADD ROWS OF COMMON NODES
72      DO 75 COL=1,BNDELM*2
          ATEMP3(1,COL)= ATEMP3(1,COL)+ATEMP3(BNDELM*RATIO*4,COL)
75      CONTINUE
      DO 85 ROW=2,BNDELM*RATIO*4-2
          PULL = 2*ROW-2
          DO 80 COL=1,BNDELM*2
              ATEMP3(ROW,COL) = ATEMP3(PULL,COL) +
1              ATEMP3(PULL+1,COL)
80      CONTINUE
85      CONTINUE
      if(.not.damat)goto 87
      write(26,7200)
      do 86 row=1,bndelm*ratio*2
          write(26,7600) (atemp3(row,col),col=1,bndelm*2)
86      continue
C FLIP RIGHT HAND GROUP OF COLUMNS
87      DO 95 ROW=1,BNDELM*RATIO*2
          DO 90 I=1,BNDELM/2
              PUSH1 = BNDELM+I
              PUSH2 = 2*BNDELM-(I-1)
              TEMP = ATEMP3(ROW,PUSH1)
              ATEMP3(ROW,PUSH1) = ATEMP3(ROW,PUSH2)
              ATEMP3(ROW,PUSH2) = TEMP
90          CONTINUE
95      CONTINUE
      if(.not.damat)goto 97

```

```

        write(26,7300)
        do 96 row=1,bndelm*ratio*2
            write(26,7600) (atemp3(row,col),col=1,bndelm*2)
96      continue
C FLIP LOWER GROUP OF ROWS
97      DO 105 COL=1,BNDELM*2
            LIMIT = (BNDELM*RATIO)/2
            DO 100 I=1,LIMIT
                PUSH1 = BNDELM*RATIO+I
                PUSH2 = BNDELM*RATIO*2-(I-1)
                TEMP = ATEMP3(PUSH1,COL)
                ATEMP3(PUSH1,COL) = ATEMP3(PUSH2,COL)
                ATEMP3(PUSH2,COL) = TEMP
100     CONTINUE
105     CONTINUE
        if(.not.damat)goto 107
        write(26,7400)
        do 106 row=1,bndelm*ratio*2
            write(26,7600) (atemp3(row,col),col=1,bndelm*2)
106     continue
C CONDENSE PHI
107     DO 115 ROW=1,BNDELM*RATIO*2
            DO 110 COL=1,BNDELM
                PULL = BNDELM+COL
                ATEMP3(ROW,COL) = ATEMP3(ROW,COL) +
                    ATEMP3(ROW,PULL)
110     CONTINUE
115     CONTINUE
        if(.not.damat)goto 117
        write(26,7500)
        do 116 row=1,bndelm*ratio*2
            write(26,7600) (atemp3(row,col),col=1,bndelm)
116     continue
C CONDENSE DISPLACEMENT
117     DO 125 COL=1,BNDELM
            DO 120 ROW=2,BNDELM*RATIO
                PULL = BNDELM*RATIO+(ROW-1)
                ATEMP3(ROW,COL) = ATEMP3(ROW,COL) +
                    ATEMP3(PULL,COL)
120     CONTINUE
125     CONTINUE
        DO 130 COL=1,BNDELM
            ATEMP3(BNDELM*RATIO+1,COL)=ATEMP3(BNDELM*RATIO*2,COL)
130     CONTINUE
        DO 132 ROW=1,INTNOD
            DO 131 COL=1,BNDELM
                ATRANS(ROW,COL)=ATEMP3(ROW,COL)
131     CONTINUE
132     CONTINUE
        if(.not.damat)RETURN
        write(26,3000)
        do 135 row=1,intnod
            write(26,7600) (atrans(row,col),col=1,bndelm)
            if(row.eq.1.or.row.eq.bndelm*ratio)write(26,6000)
135     continue
300     format(/,2x,'***** atemp transpose *****',/)
400     format(2x,100('(',2f11.6,')'))
500     format(2x,'observ =',i5)
600     format(2x,' qaobs=',f11.6,' qbobs=',f11.6)
700     format(2x,' source =',i5)

```

```

800  format(2x,'      gasrc=',f11.6,' qbsrc=',f11.6)
900  format(2x,'      atemp(1,',i3,') =',2f11.6,/,
1    2x,'      atemp(2,',i3,') =',2f11.6)
1000 format(2x,8F6.3,' |',8F6.3)
2000 format(/,2x,'***** atemp2 *****')
3000 format(/,2x,'***** atrans *****')
5000 format(2x,8F6.3)
6000 format(2x,'-----')
7000 format(/,2x,'number of points for dz integral =',i5,/,
1    2x,'number of points for dy integral =',i5)
7100 format(/,2x,'***** full a matrix *****')
7200 format(/,2x,'***** adding common nodes *****')
7300 format(/,2x,'***** flipping righthand columns *****')
7400 format(/,2x,'***** flipping lower rows *****')
7500 format(/,2x,'***** condensing out phi *****')
7600 format(2x,20F6.3)
      return
      END
C*****
C
C*****
      SUBROUTINE NORM(C,D,E,F,INT1,INT2)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four catagories:
C   1. SIZE This common block contains variables which define
C      array dimensions.
C   2. PROB This common block contains variables which define
C      problem parameters.
C   3. MAP This common block contains variables which define
C      the finite element mesh.
C   4. dbug This common block contains variables which define
C      which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare in COMMON the Gauss integration points.
C
      COMMON /INGRAL/ NUMPTY,YVALUE,WGTY,NUMPTZ,ZVALUE,WGTZ
      INTEGER NUMPTY,NMPTYD,NUMPTZ
      REAL YVALUE(100),WGTY(100),ZVALUE(100),WGTZ(100)
C
C Declare variables used only in this subroutine.

```

```

C
C      INTEGER I,ZI,YI
C      REAL    A,B,C,D,Z,Y,EPSLON,DIST,CONST
C      COMPLEX INTGYZ,INTGY,ANSY,INT1,INT2,LN,X2,DERIV
C      LOGICAL DONE
C      ++++++
C      if debug required output number of integration points.
C
C      if(dnorm)write(26,100)numpty,numptz
C      ++++++
C
C Define required constants.
C
C      CONST = 1.0/(2.0*(D-C))
C
C Initialize integrals.
C
C      INT1 = CMPLX(0.0,0.0)
C      INT2 = CMPLX(0.0,0.0)
C
C Integrate with respect to dz over each element.
C
C      Iterate through each Gauss integration point.
C
C      DO 50 ZI=1,NUMPTZ/2
C
C          Transform -1 to 1 positive integration points to c to d points.
C
C          Z = (ZVALUE(ZI)*(D-C)+D+C)/2.0
C          DONE = .FALSE.
C          GOTO 30
C
C          Transform -1 to 1 integration points to c to d points.
C          This is done after the positive point has been integrated
C          with respect to dy.
C
C      25      Z= (-ZVALUE(ZI)*(D-C)+D+C)/2.0
C          DONE = .TRUE.
C
C          For each value from the dz integral integrate with respect
C          to dy.
C
C          Initialize dy integral to zero.
C
C      30      INTGY = CMPLX(0.0,0.0)
C          ++++++
C          if(dnorm)write(26,500) zi,z
C          ++++++
C
C          Iterate through each Gauss integration point.
C
C          DO 40 YI=1,NUMPTY/2
C
C          The dy integral is divided into two integrals to
C          handle the logarithmic singularity. The first is from
C          the lower limit of the source to the z value.
C
C          A = E
C          B=Z
C
C          Transform -1 to 1 positive integration points to e to

```

z points.

Y = (YVALUE(YI)*(B-A)+B+A)/2.0

+++++

if(dnorm)write(26,550) yi,y

+++++

Evaluate derivative of Green's Function at integration points. Multiply by scaling factor and sum for total dy integral.

DIST = ABS(SIN((Z-Y)/2.0))

ANSY = DERIV(DIST)*(B-A)/2.0

+++++

if(dnorm)write(26,600)ansy

+++++

Transform -1 to 1 negative integration points to e to z points.

Y = (-YVALUE(YI)*(B-A)+B+A)/2.0

+++++

if(dnorm)write(26,550) yi,y

+++++

Evaluate derivative of Green's Function at integration points. Multiply by scaling factor and sum for total dy integral.

DIST = ABS(SIN((Z-Y)/2.0))

ANSY = ANSY + DERIV(DIST)*(B-A)/2.0

+++++

if(dnorm)write(26,600)ansy

+++++

The second portion of the dy integral is from z to f.

A=Z

B = F

+++++

if(dnorm)write(26,550) yi,y

+++++

Transform -1 to 1 positive integration points to z to f points.

Y = (YVALUE(YI)*(B-A)+B+A)/2.0

Evaluate derivative of Green's Function at integration points. Multiply by scaling factor and sum for total dy integral.

DIST = ABS(SIN((Z-Y)/2.0))

ANSY = ANSY + DERIV(DIST)*(B-A)/2.0

+++++

if(dnorm)write(26,600)ansy

+++++

Transform -1 to 1 negative integration points to z to f points.

Y = (-YVALUE(YI)*(B-A)+B+A)/2.0

+++++

if(dnorm)write(26,550) yi,y

```

C          ++++++
C          Evaluate derivative of Green's Function at integration
C          points. Multiply by scaling factor and sum for total
C          dy integral.
C
C          DIST = ABS(SIN((Z-Y)/2.0))
C          ANSY = ANSY + DERIV(DIST)*(B-A)/2.0
C          ++++++
C          if(dnorm)write(26,600)ansy
C          ++++++
C
C          Multiply dy integral by the integration weights.
C
C          INTGY = INTGY + WGTY(YI)*ANSY
C          ++++++
C          if(dnorm)write(26,650)intgy
C          ++++++
C
40      CONTINUE
C
C          Multiply dy evaluation by dz weights and scaling factors
C          and the required constants and sum to total dz integrals.
C
C          INTGYZ = CONST*WGTZ(ZI)*(D-C)/2.0*INTGY
C          INT1 = INT1 + INTGYZ*(D-Z)
C          INT2 = INT2 + INTGYZ*(Z-C)
C          IF(DONE) GOTO 50
C          GOTO 25
C
50      CONTINUE
C          ++++++
C          If debug required output value of integral.
C          if(dnorm)write(26,200) intgyz
C          ++++++
C
C          Debug format statements.
C
100     format(/2x,'number of points for DY integral =',i5,/,
1       2x,'number of points for DZ integral =',i5)
200     format(2x,'dz integral = ',2f11.6)
500     format(2x,'zi = ',i5,/,2x,'z = ',f11.6)
550     format(/,2x,'yi = ',i5,/,2x,'y = ',f11.6)
600     format(2x,'ansy = ',2f11.6)
650     format(2x,'dy integral = ',2f11.6)
C
C          Return to AMAT subroutine.
C
C          RETURN
C          END
C*****
C
C*****
C          SUBROUTINE NORM2(C,D,E,F,INT1,INT2)
C
C          Declare in COMMON all variables required by more than one
C          subroutine. These variables are divided into four categories:
C          1. SIZE This common block contains variables which define
C             array dimensions.
C          2. PROB This common block contains variables which define
C             problem parameters.
C          3. MAP This common block contains variables which define
C             the finite element mesh.

```



```

C      4. debug This common block contains variables which define
C      which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS
1  INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
1  INTEGER RATIO
1  REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
1  LOGICAL GRADNT
common /debug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
1  logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare in COMMON the Gauss integration points.
C
COMMON /INGRAL/ NUMPTY,YVALUE,WGTY,NUMPTZ,ZVALUE,WGTZ
1  INTEGER NUMPTY,NMPTYD,NUMPTZ
1  REAL YVALUE(100),WGTY(100),ZVALUE(100),WGTZ(100)
C
C Declare variables used only in this subroutine.
C
INTEGER I,ZI,YI
REAL A,B,C,D,Z,Y,E,F,DIST,CONST
COMPLEX INTGYZ,INTGY,ANSY,INT1,INT2,LN,X2,DERIV
LOGICAL DONE
C
C *****
C If debug required output number of Gauss integration points.
C
1  if(dnorm)write(26,100)numpty,numptz
1  *****
C
C Define required constant.
C
CONST = 1.0/(2.0*(D-C))
C
C Compute double Green's function integral for A matrix.
C
C
C Initialize integrals.
C
1  INT1 = CMPLX(0.0,0.0)
1  INT2 = CMPLX(0.0,0.0)
C
C Integrate with respect to dz over each element.
C
C
C Iterate through each Gauss integration point.
C
DO 50 ZI=1,NUMPTZ/2
C
C Transform -1 to 1 positive integration points to c to d points.

```

C

```

Z = (ZVALUE(ZI)*(D-C)+D+C)/2.0
DONE = .FALSE.
GOTO 30

```

C

C

C

C

C

25

```

Z= (-ZVALUE(ZI)*(D-C)+D+C)/2.0
DONE = .TRUE.

```

C

C

C

C

C

C

C

30

```

INTGY = CMPLX(0.0,0.0)

```

C

C

C

C

C

C

C

```

For each value from the dz integral integrate with respect
to dy.

```

```

Initialize dy integral to zero.

```

```

INTGY = CMPLX(0.0,0.0)

```

```

Iterate through each Gauss integration point.

```

```

DO 40 YI=1,NUMPTY/2

```

```

Define limits of integration.

```

```

A = E

```

```

B = F

```

C

C

C

C

```

Transform -1 to 1 positive integration points to e to
f points.

```

```

Y = (YVALUE(YI)*(B-A)+B+A)/2.0

```

C

C

C

C

C

```

Evaluate derivative of Green's function at integration
points. Multiply by scaling factor and sum for total
dy integral.

```

```

DIST = ABS(SIN((Z-Y)/2.0))

```

```

ANSY = DERIV(DIST)*(B-A)/2.0

```

C

C

C

C

```

Transform -1 to 1 negative integration points to e to
f points.

```

```

Y = (-YVALUE(YI)*(B-A)+B+A)/2.0

```

C

C

C

C

C

C

```

Evaluate derivative of Green's function at integration
points. Multiply by scaling factor and sum for total
dy integral.

```

```

DIST = ABS(SIN((Z-Y)/2.0))

```

```

ANSY = ANSY + DERIV(DIST)*(B-A)/2.0

```

C

C

C

```

Multiply dy integral by integration weights.

```

```

INTGY = INTGY + WGTY(YI)*ANSY

```

40

```

CONTINUE

```

C

C

C

```

Multiply dy evaluation by dz weights and scaling factors
and the required constants and sum to total dz integrals.

```

```

C
      INTGYZ = CONST*WGTZ(ZI)*(D-C)/2.0*INTGY
      INT1 = INT1 + INTGYZ*(D-Z)
      INT2 = INT2 + INTGYZ*(Z-C)
      IF(DONE) GOTO 50
      GOTO 25
50  CONTINUE
C *****
C If debug required output values of integrals.
C
      if(dnorm)write(26,200) intgyz
      if(dnorm)write(26,1100) int1,int2
C *****
C
C Debug format statements.
C
100  format(/2x,          number of points for DY integral =',i5,/,
1    2x,'          number of points for DZ integral =',i5)
200  format(2x,'          integral = ',2f11.6)
1100 format(2x,'          int1 =',2f11.6,/,
      2x,'          int2 =',2f11.6)
C
C Return to AMAT subroutine.
C
      RETURN
      END
C *****
C *****
      COMPLEX FUNCTION DERIV(DIST)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C      array dimensions.
C   2. PROB This common block contains variables which define
C      problem parameters.
C   3. MAP This common block contains variables which define
C      the finite element mesh.
C   4. dbug This common block contains variables which define
C      which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1      NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
1      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1      LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
1      INTEGER RATIO
1      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
1      LOGICAL GRADNT
      common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1      dhspac,direct,dtri,dgamma,dfilam,damat,dbmat,
1      dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
1      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1      direct,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1      ddiag,ddiag2,dfunc,dderiv,dctest,datest

```

```

C
C Declare variables used in this function only.
C
      REAL    KAPPA,X,DIST,ARG,F1,THETA,Y1,J1
C
C Define necessary constant.
C
      KAPPA = 'SQRT(W2*RANGE/EXTG)
C
C Compute argument of Green's function derivative.
C
      X = 2.0*KAPPA*RANGE*DIST
C
C Test argument to determine proper formula for computation.
C
      IF(X.LT.3.0) GOTO 10
C
C Compute derivative of Green's function.
C
      ARG = 3.0/X
      F1 = (((((-0.00020033*ARG+.00113653)*ARG-.00249511)*ARG
1      +.00017105)*ARG+.01659667)*ARG+.00000156)*ARG
1      +.79788456
      THETA = (((((-0.00029166*ARG+.00079824)*ARG+.00074348)*ARG
1      -.00637879)*ARG+.00005650)*ARG+.12499612)*ARG
1      -2.35619449+X
      J1 = F1*COS(THETA)/SQRT(X)*KAPPA*DIST/(-4.0)
      Y1 = F1*SIN(THETA)/SQRT(X)*KAPPA*DIST/(4.0)
      ++++++
C
C If debug desired output computed values.
C
      if(dderiv)write(26,500)kappa,dist,x,j1,y1
      ++++++
      DERIV = CMPLX(Y1,J1)
C
C Return to NORM or NORM2 subroutines.
C
      RETURN
C
C Compute derivative of Green's function.
C
10  ARG = (X/3.0)**2
      F1 = ((((((0.00001109*ARG-.00031761)*ARG+.00443319)*ARG
1      -.03954289)*ARG+.21093573)*ARG-.56249985)*ARG+0.5)*X
      THETA = ((((((0.0027873*ARG-.0400976)*ARG+.3123951)*ARG
1      -1.3164827)*ARG+2.1682709)*ARG+.2212091)*ARG
1      -.6366198+2/3.1415927*X*ALOG(0.5*X)*F1)/X
      J1 = F1*KAPPA*DIST/(-4.0)
      Y1 = THETA*KAPPA*DIST/(4.0)
      ++++++
C
C If debug desired output computed values.
C
      if(dderiv)write(26,500)kappa,dist,x,j1,y1
      ++++++
      DERIV = CMPLX(Y1,J1)
C
C Return to NORM or NORM2 subroutines.
C
      RETURN
C

```

C Debug format statements.

```
C
500  format(2x,'kappa = ',f11.6,/,
1    2x,'distance = ',f11.6,/,
1    2x,'x = ',f11.6,/,
1    2x,'j1 = ',f11.6,/,
1    2x,'y1 = ',f11.6,/,
1    2x,'func = cmplx(y1,j1)')
      END
```

C*****

C

C*****

SUBROUTINE ATEST(ATRANS,FG,BMATRX)

C

C Declare in COMMON all variables required by more than one

C subroutine. These variables are divided into four categories:

C 1. SIZE This common block contains variables which define

C array dimensions.

C 2. PROB This common block contains variables which define

C problem parameters.

C 3. MAP This common block contains variables which define

C the finite element mesh.

C 4. debug This common block contains variables which define

C which debug switches are desired.

C Arrays are not passed through COMMON but passed as arguments to the

C subroutines.

C

```
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1          NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1          LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /debug/ dmain,dmesh,dassm,dktest,dforce,
1          dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1          dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1          drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1          ddiag,ddiag2,dfunc,dderiv,dctest,datest
      INTEGER COL1,COL2,ROW,IER
      REAL WA(15),BMATRX(BNDELM,BCOLS),TMPB(15,15),TMPB(15,16)
      COMPLEX ATRANS(INTNOD,BNDELM),
1          FG(INTNOD),TMPA(15,15),TMPFG(15),ANS(15),TMPA(15,16)
1          ,TMPAT(16,15),TMPAAT(15,15)
      WRITE(26,2000)
      IF(INTNOD.GT.16.OR.BNDELM.GT.15) GOTO 100
```

C Write BMATRX

```
      WRITE(26,1100)
```

```
      DO 5 ROW=1,BNDELM
```

```
          WRITE(26,1000) (BMATRX(ROW,COL1),COL1=1,BCOLS)
```

```
5      CONTINUE
```

C WRITE ATRANS

```
      WRITE(26,1200)
```

```
      DO 10 ROW=1,INTNOD
```

```
          WRITE(26,1000) (ATrans(ROW,COL1),COL1=1,BNDELM)
```

```
10     CONTINUE
```

```

C COPY ATRANS
  DO 12 ROW=1,INTNOD
    DO 11 COL1=1,BNDELM
      TMPAT(ROW,COL1)=ATrans(ROW,COL1)
    11 CONTINUE
  12 CONTINUE
C WRITE COPY OF ATRANS
  WRITE(26,1900)
  DO 13 ROW=1,INTNOD
    WRITE(26,1000) (TMPAT(ROW,COL1),COL1=1,BNDELM)
  13 CONTINUE
C ADD BMATRIX TERM TO ATRANS
  DO 20 ROW=1,BNDELM
    DO 15 COL1=1,BCOLS
      COL2=RATIO*(ROW-1)+COL1
      TMPAT(COL2,ROW)=ATrans(COL2,ROW)+
        EXTG*ALPHA/G*BMATRIX(ROW,COL1)
    15 CONTINUE
  20 CONTINUE
C WRITE ATRANS WITH BMATRIX TERM ADDED
  WRITE(26,1300)
  DO 25 ROW=1,INTNOD
    WRITE(26,1000) (TMPAT(ROW,COL1),COL1=1,BNDELM)
  25 CONTINUE
C MULTIPLY A * A TRANSPOSE
  DO 40 COL1=1,BNDELM
    DO 35 ROW=1,BNDELM
      TMPAAT(ROW,COL1)=CMPLX(0.0,0.0)
      DO 30 COL2=1,INTNOD
        TMPAAT(ROW,COL1)=TMPAAT(ROW,COL1)+
          TMPAT(COL2,ROW)*TMPAT(COL2,COL1)
      30 CONTINUE
    35 CONTINUE
  40 CONTINUE
C WRITE A * A TRANSPOSE
  WRITE(26,1400)
  DO 45 ROW=1,BNDELM
    WRITE(26,1000) (TMPAAT(ROW,COL1),COL1=1,BNDELM)
  45 CONTINUE
C MULTIPLY A * FG
  DO 55 ROW=1,BNDELM
    TMPFG(ROW)=CMPLX(0.0,0.0)
    DO 50 COL2=1,INTNOD
      TMPFG(ROW)=TMPFG(ROW)+
        TMPAT(COL2,ROW)*FG(COL2)
    50 CONTINUE
  55 CONTINUE
C WRITE A * FG
  WRITE(26,1500)
  DO 60 ROW=1,BNDELM
    WRITE(26,1000) TMPFG(ROW)
  60 CONTINUE
C SOLVE FOR PHI
  CALL LEQTLQ(TMPAAT,BNDELM,15,TMPFG,1,15,0,WA,IER)
  IF(IER.EQ.129) GOTO 110
C WRITE PHI
  WRITE(26,1600)
  DO 65 ROW=1,BNDELM
    WRITE(26,1000) TMPFG(ROW)
  65 CONTINUE

```

```

        WRITE(26,2000)
        RETURN
100    WRITE(26,1700)
        STOP
110    WRITE(26,1800)
        STOP
2000   FORMAT(/,2X,'ATEST SUBROUTINE-----')
1900   FORMAT(/,2X,'***** COPIED ATRANS *****')
1800   FORMAT(/,2X,'A * A TRANSPOSE IS SINGULAR.')
1700   FORMAT(/,2X,'MATRICES ARE LARGER THAN THE TEMPORARY STORAGE
1    IN ATEST.',/,2X,'EXECUTION ABORTED')
1600   FORMAT(/,2X,'***** PHI *****')
1500   FORMAT(/,2X,'***** A * FG *****')
1400   FORMAT(/,2X,'***** A*A TRANSPOSE *****')
1300   FORMAT(/,2X,'***** ATRANS + B TERM *****')
1200   FORMAT(/,2X,'***** ATRANS *****')
1100   FORMAT(/,2X,'***** BMATRX *****')
1000   FORMAT(2X,100F11.6)
        END
C*****
C
C*****
        SUBROUTINE CMAT(C,CTEMP)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C     1. SIZE This common block contains variables which define
C         array dimensions.
C     2. PROB This common block contains variables which define
C         problem parameters.
C     3. MAP This common block contains variables which define
C         the finite element mesh.
C     4. dbug This common block contains variables which define
C         which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
        COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1    NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
        INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1    LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
        COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
        REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
        COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
        INTEGER RATIO
        REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
        LOGICAL GRADNT
        common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1    dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1    dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
        logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1    drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1    ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare in COMMON the Gauss integration points.
C
        COMMON /INGRAL/ NUMPTY,YVALUE,WGTY,NUMPTZ,ZVALUE,WGTZ
        INTEGER NUMPTY,NUMPTYD,NUMPTZ
        REAL YVALUE(100),WGTY(100),ZVALUE(100),WGTZ(100)
C

```

```

C Declare and dimension arrays required in this subroutine.
C
      COMPLEX C(BNDELM,BNDELM),CTEMP(NUMANG)
C
C Declare variables used only in this subroutine.
C
      INTEGER I,ROW,COL,SOURCE,PULL1,PULL2
      REAL    QAOBS,QBOBS,QASRC,QBSRC
C
C Perform double integral of Green's function.
C
C
C Determine limits of integration for outer integral. This is the
C integral over the observer.
C
      QAOBS = 0.0
      QBOBS = BDANGL
C
C Perform integral over first source.
C
      SOURCE = 1
C
C Read in the Gauss integration points desired.
C
      READ(24,*)NUMPTY
      DO 10 I=1,NUMPTY/2
        READ(24,*) YVALUE(I),WGTY(I)
10      CONTINUE
      READ(24,*)NUMPTZ
      DO 20 I=1,NUMPTZ/2
        READ(24,*) ZVALUE(I),WGTZ(I)
20      CONTINUE
C
C Evaluate integral.
C
      CALL DIAG(QAOBS,QBOBS,CTEMP(SOURCE))
C
C *****
C If debug desired compute exact integral for  $\ln|z-y|$  and
C output.
C
      if(dcmat)exact=(qaobs-qbobs)*(qbobs-qaobs)+(qbobs-qaobs)**2
1      *(alog(qbobs-qaobs)-0.5)+qbobs*(1.0-alog(qbobs-qaobs))*
1      (qbobs-qaobs-1.0)
      if(dcmat)write(26,600) exact
      if(dcmat)write(26,500) source,ctemp(source)
C
C *****
C
C Perform integral over second source.
C
      SOURCE = 2
C
C Read in the Gauss integration points desired.
C
      READ(24,*)NUMPTY
      DO 40 I=1,NUMPTY/2
        READ(24,*) YVALUE(I),WGTY(I)
40      CONTINUE
      READ(24,*)NUMPTZ
      DO 50 I=1,NUMPTZ/2
        READ(24,*) ZVALUE(I),WGTZ(I)

```


50

CONTINUE

Determine limits of integration for second source.

QASRC = (SOURCE-1)*BDANG1
QBSRC = SOURCE*BDANG1

Evaluate integral

CALL DIAG2(QAOBS,QBOBS,QASRC,QBSRC,CTEMP(SOURCE))
++++
If debug desired compute exact integral for $\ln|z-y|$ and
output.

if(dcmat)exact=-.5*(qbsrc-qboobs)**2*alog(qbsrc-qboobs)+.75*
1 (qbsrc-qboobs)**2+.5*qbsrc**2*alog(qbsrc)-.75*qbsrc**2+
1 -1.0*(.75*
1 (qasrc-qboobs)**2+.5*qasrc**2*alog(qasrc)-.75*qasrc**2)
if(dcmat)write(26,600) exact
if(dcmat)write(26,500) source,ctemp(source)
++++

Read in Gauss integration points for remaining sources.

READ(24,*)NUMPTY
DO 60 I=1,NUMPTY/2
 READ(24,*) YVALUE(I),WGTY(I)
60 CONTINUE
 READ(24,*)NUMPTZ
 DO 70 I=1,NUMPTZ/2
 READ(24,*) ZVALUE(I),WGTZ(I)
70 CONTINUE

Perform integral over remaining sources.

DO 80 SOURCE=3,BNDELM + 1

Determine limits of integration.

QASRC = (SOURCE-1)*BDANG1
QBSRC = SOURCE*BDANG1

Evaluate integral.

CALL DIAG2(QAOBS,QBOBS,QASRC,QBSRC,CTEMP(SOURCE))
++++
If debug desired compute exact integral for $\ln|z-y|$ and
output.

if(dcmat)exact=-.5*(qbsrc-qboobs)**2*alog(qbsrc-qboobs)+.75*
1 (qbsrc-qboobs)**2+.5*qbsrc**2*alog(qbsrc)-.75*qbsrc**2+
1 -1.0*(-.5*(qasrc-qboobs)**2*alog(qasrc-qboobs)+.75*
1 (qasrc-qboobs)**2+.5*qasrc**2*alog(qasrc)-.75*qasrc**2)
if(dcmat)write(26,600) exact
if(dcmat)write(26,500) source,ctemp(source)
++++
80 CONTINUE
++++
if(dcmat)write(26,400) (i,i=1,bndelm)
++++

C
C Position observer one integrals into proper place in C matrix. This is
C done on the basis of a circulant matrix which is then condensed to
C reflect only a half-circle.

```

C
      DO 100 ROW=1,BNDELM
        DO 90 COL=1,BNDELM
          IF(COL.LT.ROW) GOTO 85
          PULL1 = COL-(ROW-1)
          PULL2 = COL + ROW
          IF(PULL2.GT.BNDELM+1) PULL2=2*(BNDELM+1)-PULL2
          C(ROW,COL) = 2.0*(CTEMP(PULL1) + CTEMP(PULL2))
          GOTO 90
        85      C(ROW,COL) = C(COL,ROW)
        90      CONTINUE
C
C *****
C      IF(DCMAT)WRITE(26,300) ROW,(C(ROW,COL),COL=1,BNDELM)
C *****
C 100  CONTINUE
C
C Debug format statements.
C
C 300  format(1x,i2,1x,100(1x,2f6.3))
C 400  format(//2x,'***** full c matrix *****',//
C      1  ,11x,100(i2,11x))
C 500  format(2x,'ctemp(',i3,') = ',2f11.6,/)
C 600  format(2x,'exact ln|z-y| integral = ',f11.6)
C
C Return to HSPACE subroutine.
C
      RETURN
      END

```

C*****
SUBROUTINE DIAG(C,D,INTGYZ)

C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C 1. SIZE This common block contains variables which define
C array dimensions.
C 2. PROB This common block contains variables which define
C problem parameters.
C 3. MAP This common block contains variables which define
C the finite element mesh.
C 4. debug This common block contains variables which define
C which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.

```

C
COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
INTEGER RATIO
REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
LOGICAL GRADNT

```

```

common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1 dhspac,direct,dtri,dgamma,dfilam,damat,dbmat,
1 dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1 direct,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1 ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare in COMMON the Gauss integration points.
C
COMMON /INGRAL/ NUMPTY,YVALUE,WGTY,NUMPTZ,ZVALUE,WGTZ
INTEGER NUMPTY,NMPTYD,NUMPTZ
REAL YVALUE(100),WGTY(100),ZVALUE(100),WGTZ(100)
C
C Declare variable used only int this subroutine.
C
INTEGER I,ZI,YI
REAL A,B,C,D,Z,Y,EPSLON,DIST,CONST
COMPLEX INTGYZ,INTGY,ANSY,FUNC
LOGICAL DONE
C *****
C If debug desired output number of Gauss integration points.
C
if(ddiag)write(26,100)numpty,numptz
C *****
C Define required constant
C
CONST = -0.5
C
C Compute double Green's function integral for C matrix.
C
C Initialize integral
C
INTGYZ = CMPLX(0.0,0.0)
C
C Integrate with respect to dz over each element.
C
C Iterate through each Gauss integration point.
C
DO 50 ZI=1,NUMPTZ/2
C
C Transform -1 to 1 positive integration points to c to d points
C
Z = (ZVALUE(ZI)*(D-C)+D+C)/2.0
DONE = .FALSE.
GOTO 30
C
C Transform -1 to 1 negative integration points to c to d
C points. This is done after the positive point has been
C integrated with respect to dy.
C
25 Z= (-ZVALUE(ZI)*(D-C)+D+C)/2.0
DONE = .TRUE.
C
C For each value from the dz integral integrate with respect to dy.
C
C Initialize dy integral to zero.

```

```
INTGY = CMPLX(0.0,0.0)
```

Iterate through each Gauss integration point.

```
DO 40 YI=1,NUMPTY/2
```

The dy integral is divide into two integrals to handle the logarithmic singularity. The first is from the lower limit to the z value.

```
A = C
B=Z
```

Transform -1 to 1 positive integration points to c to z points.

```
Y = (YVALUE(YI)*(B-A)+B+A)/2.0
```

Evaluate Green's function at integration points. Multiply by scaling factor and sum for total dy integral.

```
DIST = 2.0*RANGE*ABS(SIN((Z-Y)/2.0))
ANSY = FUNC(DIST)*(B-A)/2.0
```

Transform -1 to 1 negative integration points to c to z points.

```
Y = (-YVALUE(YI)*(B-A)+B+A)/2.0
DIST = 2.0*RANGE*ABS(SIN((Z-Y)/2.0))
```

Evaluate Green's function at integration points. Multiply by scaling factor and sum for total dy integral.

```
ANSY = ANSY + FUNC(DIST)*(B-A)/2.0
```

The second portion of the dy integral is from z to d.

```
A=Z
B = D
```

Transform -1 to 1 positive integration points to c to z points.

```
Y = (YVALUE(YI)*(B-A)+B+A)/2.0
```

Evaluate Green's function at integration points. Multiply by scaling factor and sum for total dy integral.

```
DIST = 2.0*RANGE*ABS(SIN((Z-Y)/2.0))
ANSY = ANSY + FUNC(DIST)*(B-A)/2.0
```

Transform -1 to 1 negative integration points to c to z points.

```
Y = (-YVALUE(YI)*(B-A)+B+A)/2.0
```

```

C
C      Evaluate Green's function at integration points.
C      Multiply by scaling factor and sum for total dy
C      integral.
C
C          DIST = 2.0*RANGE*ABS(SIN((Z-Y)/2.0))
C          ANSY = ANSY + FUNC(DIST)*(B-A)/2.0
C
C      Multiply dy integral by the integration weights.
C
C          INTGY = INTGY + WGTY(YI)*ANSY
40      CONTINUE
C
C      Multiply dy evaluation by dz weights and scaling factors
C      and the required constant and sum to total dz integral.
C
C          INTGYZ = INTGYZ + CONST*WGTZ(ZI)*(D-C)/2.0*INTGY
C          IF(DONE) GOTO 50
C          GOTO 25
50      CONTINUE
C      ++++++
C      If debug desired output value of integral.
C
C          if(ddiag)write(25,200) intgyz
C          ++++++
C      Debug format statements.
C
100     format(/2x,'number of points for DY integral =',i5,/,
1       2x,'number of points for DZ integral =',i5)
200     format(2x,'integral = ',2f11.6)
C
C      Return to CMAT subroutine.
C
C          RETURN,
C          END
C*****
C      SUBROUTINE DIAG2(C,D,E,F,INTGYZ)
C
C      Declare in COMMON all variables required by more than one
C      subroutine. These variables are divided into four categories:
C      1. SIZE This common block contains variables which define
C          array dimensions.
C      2. PROB This common block contains variables which define
C          problem parameters.
C      3. MAP This common block contains variables which define
C          the finite element mesh.
C      4. dbug This common block contains variables which define
C          which debug switches are desired.
C      Arrays are not passed through COMMON but passed as arguments to the
C      subroutines.
C
C          COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1         NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
C          INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1         LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
C          COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
C          REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
C          COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
C          INTEGER RATIO

```

```

      REAL    SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common  /dbug/ dmain,dmesh,dassm,dktest,dforce,
1            dhspac,direct,dtri,dgamma,dfilam,damat,dbmat,
1            dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1            direct,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1            ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare in COMMON the Gauss integration points.
C
      COMMON /INGRAL/ NUMPTY,YVALUE,WGTY,NUMPTZ,ZVALUE,WGTZ
      INTEGER NUMPTY,NMPTYD,NUMPTZ
      REAL    YVALUE(100),WGTY(100),ZVALUE(100),WGTZ(100)
C
C Declare variables used only in this subroutine.
C
      INTEGER I,ZI,YI
      REAL    A,B,C,D,Z,Y,EPSLON,E,F,DIST,CONST
      COMPLEX INTGYZ,INTGY,ANSY,FUNC
      LOGICAL DONE
      ++++++
C If debug desired output number of Gauss integration points.
C
      if(ddiag2)write(26,100)numpty,numptz
      ++++++
C
C Define required constant
C
      CONST = -0.5
C
C Compute double Green's function integral for C matrix.
C
C Initialize integral
C
      INTGYZ = CMPLX(0.0,0.0)
C
C Integrate with respect to dz over each element.
C
C Iterate through each Gauss integration point.
C
      DO 50 ZI=1,NUMPTZ/2
C
C      Transform -1 to 1 positive integration points to c to d points
C
C      Z = (ZVALUE(ZI)*(D-C)+D+C)/2.0
C      DONE = .FALSE.
C      GOTO 30
C
C      Transform -1 to 1 negative integration points to c to d
C      points. This is done after the positive point has been
C      integrated with respect to dy.
C
25      Z= (-ZVALUE(ZI)*(D-C)+D+C)/2.0
C      DONE = .TRUE.
C
C      For each value from the dz integral integrate with respect to dy.
C

```

```

C
C
C
30      Initialize dy integral to zero.
C
C      INTGY = CMPLX(0.0,0.0)
C
C      Iterate through each Gauss integration point.
C
C      DO 40 YI=1,NUMPTY/2
C
C      Define limits of integration.
C
C          A = E
C          B = F
C
C      Transform -1 to 1 positive integration points to c to
C      z points.
C
C          Y = (YVALUE(YI)*(B-A)+B+A)/2.0
C
C      Evaluate Green's function at integration points.
C      Multiply by scaling factor and sum for total dy
C      integral.
C
C          DIST = 2.0*RANGE*ABS(SIN((Z-Y)/2.0))
C          ANSY = FUNC(DIST)*(B-A)/2.0
C
C      Transform -1 to 1 negative integration points to c to z
C      points.
C
C          Y = (-YVALUE(YI)*(B-A)+B+A)/2.0
C
C      Evaluate Green's function at integration points.
C      Multiply by scaling factor and sum for total dy
C      integral.
C
C          DIST = 2.0*RANGE*ABS(SIN((Z-Y)/2.0))
C          ANSY = ANSY + FUNC(DIST)*(B-A)/2.0
C
C      Multiply dy integral by the integration weights.
C
C          INTGY = INTGY + WGTY(YI)*ANSY
40      CONTINUE
C
C      Multiply dy evaluation by dz weights and scaling factors
C      and the required constant and sum to total dz integral.
C
C          INTGYZ = INTGYZ + CONST*WGTZ(ZI)*(D-C)/2.0*INTGY
C          IF(DONE) GOTO 50
C          GOTO 25
50      CONTINUE
C      ++++++
C      If debug desired output value of integral.
C
C          if(ddiag2)write(26,200) intgyz
C          ++++++
C
C      Debug format statements.
C
100     format(/2x,'number of points for DY integral =',i5,/,
1       2x,'number of points for DZ integral =',i5)

```

```

200  format(2x,'integral = ',2f11.6)
C
C Return to CMAT subroutine.
C
      RETURN
      END
C*****
      COMPLEX FUNCTION FUNC(DIST)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C      array dimensions.
C   2. PROB This common block contains variables which define
C      problem parameters.
C   3. MAP This common block contains variables which define
C      the finite element mesh.
C   4. dbug This common block contains variables which define
C      which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1          dhspac,direct,dtri,dgamma,dfilam,damat,dbmat,
1          dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1          direct,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1          ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare variables used in this function only.
C
      REAL KAPPA,DIST,X,ARG,FO,THETA,YO,JO
C
C Define necessary constant.
C
      KAPPA = SQRT(W2*RANGE/EXTG)
C
C Compute Green's function argument.
C
      X = KAPPA*DIST
C
C Test argument to determine proper formula for computation.
C
      IF(X.LT.3.0)GOTO 10
C
C Compute Green's function
C
      ARG = 3.0/X
      FO=((((0.00014476*ARG-.00072805)*ARG+.0013723)*ARG
1      -.00009512)*ARG-.00552740)*ARG-.00000077)*ARG+.79788456
      THETA=((((0.00013558*ARG-.00029333)*ARG-.00054125)*ARG
1      +.00262573)*ARG-.00003954)*ARG-.04166397)*ARG
1      -.78539816+X
      JO = X*-0.5*FO*COS(THETA)/(4.0)

```



```

      YO = X**(-0.5*FO*SIN(THETA))/(-4.0)
      ++++++
C If debug desired output computed values.
C
      if(dfunc)write(26,500)kappa,dist,x,j0,y0
      ++++++
      FUNC = CMPLX(YO,J0)
C
C Return to DIAG or DIAG2 subroutines.
C
      RETURN
C
C Compute Green's function
C
10  ARG = (X/3.0)**2
      FO((((0.0002100*ARG-.0039444)*ARG+.0444479)*ARG
1   -.3163866)*ARG+1.2656208)*ARG-2.2499997)*ARG+1.0
      THETA(((((-.00024846*ARG+.00427916)*ARG-.04261214)*ARG
1   +.25300117)*ARG-.74350384)*ARG+.60559366)*ARG
1   +.36746691+2.0/3.14159265*ALOG(0.5*X)*FO
      JO = FO/(4.0)
      YO = THETA/(-4.0)
      ++++++
C If debug desired output computed values.
C
      if(dfunc)write(26,500)kappa,dist,x,j0,y0
      ++++++
      FUNC = CMPLX(YO,J0)
C
C Return to DIAG or DIAG2 subroutines.
C
      RETURN
C
C Debug format statements.
C
500  format('/',2x,'kappa = ',f11.6,/,
1    2x,'distance = ',f11.6,/,
1    2x,'x = ',f11.6,/,
1    2x,'j0 = ',f11.6,/,
1    2x,'y0 = ',f11.6,/,
1    2x,'func = cmplx(y0,j0)')
      END
C*****
C
C*****
      SUBROUTINE CTEST(FPHI,C)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C   1. SIZE This common block contains variables which define
C      array dimensions.
C   2. PROB This common block contains variables which define
C      problem parameters.
C   3. MAP This common block contains variables which define
C      the finite element mesh.
C   4. dbug This common block contains variables which define
C      which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C

```

```

COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
1  INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETAO
REAL W2,GA,GB,RO,EXTG,ALPHA,THETAO
COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
INTEGER RATIO
REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
LOGICAL GRADNT
common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1  dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1  dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
1  logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1  drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1  ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Declare and dimension arrays used in this subroutine.
C
REAL WA(15)
COMPLEX C(BNDELM,BNDELM),SUM,W,FPHI(BNDELM),
1  FUNC,TEMPC(15,15),TMPFHI(15),ANS(15)
C
C Declare variables used only in this subroutine.
C
INTEGER I,IER
WRITE(26,600)
C
C Copy C matrix and force vector so test can be performed without
C damage. Also initialize result.
C
DO 4 I=1,BNDELM
DO 5 J=1,BNDELM
TEMPC(I,J)=C(I,J)
5  CONTINUE
TMPFHI(I)=FPHI(I)
ANS(I)=CMPLX(0.0,0.0)
4  CONTINUE
C
C Solve equation C*PHI= FPHI
C
CALL LEQ1C(TEMPC,BNDELM,15,TMPFHI,1,15,0,WA,IER)
IF(IER.EQ.129) GOTO 90
WRITE(26,150)
C
C Sum phi's. Displacement at origin equals G(0,y)*delta theta*sum of phji's.
C
SUM = CMPLX(0.0,0.0)
DO 10 I=1,BNDELM
WRITE(26,200) I,TMPFHI(I)
SUM = SUM + TMPFHI(I)
10  CONTINUE
WRITE(26,550)
C
C Multiply PHI*C to see if C matrix is well behaved.
C
DO 20 I=1,BNDELM
DO 30 J=1,BNDELM
ANS(I)=ANS(I)+C(I,J)*TMPFHI(J)
30  CONTINUE

```

```

        WRITE(26,500) I,ANS(I),FPHI(I)
20  CONTINUE
C
C Determine G(0,y).
C
        W = FUNC(RANGE)
        WRITE(26,650) W
C
C Determine displacement at origin.
C
        W = 2.0 * BDANG1 * SUM * W
        WRITE(26,250) W
        WRITE(26,600)
C
C Return to HSPACE subroutine.
C
        RETURN
90  WRITE(5,100)
    STOP
C
C Debug format statements.
C
100  FORMAT(/,2X,'C MATRIX IS SINGULAR. EXECUTION ABORTED.',/)
125  FORMAT(/2X,'MATRICES ARE LARGER THAN THE TEMPORARY STORAGE IN
1  CTEST.',//,2X,'EXECUTION ABORTED.')
150  FORMAT(/,2X,'ELEMENT',11X,'PHI',/)
200  FORMAT(2X,I5,5X,2F11.6)
250  FORMAT(/,2X,'DISPLACEMENT AT ORIGIN = ',2F11.6)
550  FORMAT(/,2X,'ELEMENT',11X,'ANS',22X,'FPHI',/)
500  FORMAT(2X,I5,5X,2F11.6,5X,2F11.6)
600  FORMAT(2X,'SUBROUTINE CTEST -----',/)
650  FORMAT(/2X,'G(R) = ',2F11.6)
    END
C*****
C
C*****

        SUBROUTINE SOLVE(K,D,FG,FD,KOG,KOO,B,WHOLE,SLTN,W,XL,WA,
1  LAM,TEMPD,CINVER,FPHI)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four categories:
C
C 1. SIZE This common block contains variables which define
C    array dimensions.
C
C 2. PROB This common block contains variables which define
C    problem parameters.
C
C 3. MAP This common block contains variables which define
C    the finite element mesh.
C
C 4. dbug This common block contains variables which define
C    which debug switches are desired.
C
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
        COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1  NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
        INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1  LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
        COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
        REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
        COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT

```

```

      INTEGER RATIO
      REAL    SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /dbug/ dmain,dmesh,dassm,dktest,dforce,
1          dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1          dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical .dmain,dmesh,dassm,dktest,dforce,dhspac,
1          drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1          ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Dimension and declare arrays used within this subroutine.
C
      REAL    K(NUMNOD,WIDTH),KOG(NUMEQN,INTNOD),KOO(NUMEQN,WIDTH),
1          B(NUMEQN,INTNOD),XL(NUMEQN,SPACE),WA(INTNOD)
      COMPLEX D(INTNOD,INTNOD),FG(INTNOD),FD(INTNOD),SLTN(INTNOD),
1          WHOLE(INTNOD,INTNOD),W(INTNOD),LAM(BNDELM),
1          TEMPD(INTNOD,INTNOD),CINVER(BNDELM,BNDELM),FPHI(BNDELM)
C
C Declare variables used only by this subroutine.
C
      INTEGER ROW,COL,COL1,COL2,PULL,IER,N,L,M,I,J,P
      REAL    KAPPA,KAPPAR,THETA

C$      WRITE(26,700)
C
C Partition K(omega,gamma) from structure stiffness matrix. KOG is
C pulled term by term from K. KOG is stored in full storage mode.
C
      N=0
      DO 20 I=INTNOD+1,NUMNOD
          N=N+1
          DO 10 J=1,INTNOD
              KOG(N,J)=0.0
              B(N,J)=0.0
              M=I-(1+CODIAG)
              PULL=J-M
              IF(PULL.LE.0) GOTO 10
              IF(PULL.GT.WIDTH) GOTO 20
              KOG(N,J)=K(I,PULL)
              B(N,J)=K(I,PULL)*-1.0
10          CONTINUE
20      CONTINUE
C$      write(26,1300)
C$      DO 53 ROW=1,NUMEQN
C$          WRITE(26,1200) (KOG(ROW,COL),COL=1,INTNOD)
C$      53 CONTINUE
C$      write(26,1400)
C$      DO 63 ROW=1,NUMEQN
C$          WRITE(26,1200) (B(ROW,COL),COL=1,INTNOD)
C$      63 CONTINUE
C
C Partition K(omega,omega) from structure stiffness matrix. KOO is
C pulled term by term from K. KOO is stored in band storage mode rather
C than symmetric storage mode to allow the use of an IMSL solving
C routine.
C
      DO 40 I=INTNOD+1,NUMNOD
          N=I-(INTNOD+1+CODIAG)
          P=N
          IF(N.LT.0)N=0

```

```

      M=I+CODIAG
      IF (M.GT.NUMNOD) M=NUMNOD
      DO 30 J=INTNOD+1+N,M
          L=I-(1+CODIAG)
          PULL=J-L
          ROW=I-INTNOD
          COL=J-INTNOD-P
          KOO(ROW,COL)=K(I,PULL)
30      CONTINUE
40      CONTINUE
C$      write(26,1500)
C$      do 74 i=1,numeqn
C$          write(26,1200) (koo(i,j),j=1,WIDTH)
C$ 74      continue
C
C Solve equation KOO x X = B = -KOG. X, the solution is written over
C top of B. This solving is done with IMSL routine LEQT1B.
C
      CALL LEQT1B(KOO,NUMEQN,CODIAG,CODIAG,NUMEQN,B,INTNOD,NUMEQN,0,
1      XL,IER)
      IF (IER.EQ.129) write(5,400)
400      format(2x,'error')
C$      write(26,1600)
C$      do 73 i=1,numeqn
C$          write(26,1200) (b(i,j),j=1,intnod)
C$ 73      continue
C
C Multiply k(gamma,omega) times -K(omega,omega) inverse times
C K(omega,gamma).
C
      DO 50 COL=1,INTNOD
          DO 60 ROW=1,INTNOD
              KOO(ROW,COL)=0.0
              DO 70 COL2=1,NUMEQN
                  KOO(ROW,COL) = KOO(ROW,COL) +
1                  KOG(COL2,ROW)*B(COL2,COL)
70      CONTINUE
60      CONTINUE
50      CONTINUE
C$      write(26,1100)
C$      do 51 row=1,intnod
C$          write(26,1200) (koo(row,col),col=1,intnod)
C$ 51      continue
C
C Assemble WHOLE matrix.
C
      DO 80 ROW=1,INTNOD
          DO 90 COL=1,INTNOD
C
C      Load K(gamma,gamma)
C
          L=ROW-(1+CODIAG)
          PULL=COL-L
          IF (PULL.LT.0.OR.PULL.GT.WIDTH) GOTO 91
          PULL = COL+ROW*(ROW-1)/2
          IF (COL.GT.ROW) PULL = ROW+COL*(COL-1)/2
          WHOLE(ROW,COL)=K(ROW,PULL)
          GOTO 93
91      WHOLE(ROW,COL)=CMPLX(0.0,0.0)
C

```

```

700  FORMAT(2X,'SUBROUTINE SOLVE -----')
800  format(2x,'row = ',I3,2x,'theta = ',f5.3,2x,'kappa = ',f5.3)
900  format(2x,'w(',I3,') = ',2f15.6)
1000 format(1x,'fg = ',2f10.6,' fd = ',2f10.6,' sltn = ',2f10.6)
1100 format(/,2x,'*****'
1  -K(GAMMA,OMEGA)*K(OMEGA,OMEGA)-1*K(OMEGA,GAMMA) *****',/)
1200 format(1x,100f7.4)
1300 format(/,2x,'kog')
1400 format(/,2x,'b')
1500 format(/,2x,'koo')
1600 format(/,2x,'solution matrix')
C
C Return to MAIN program.
C
      RETURN
      END
C*****
C
C*****
      SUBROUTINE OUT(SLTN,W,FG,FI,X,LAM)
C
C Declare in COMMON all variables required by more than one
C subroutine. These variables are divided into four catagories:
C 1. SIZE This common block contains variables which define
C    array dimensions.
C 2. PROB This common block contains variables which define
C    problem parameters.
C 3. MAP This common block contains variables which define
C    the finite element mesh.
C 4. debug This common block contains variables which define
C    which debug switches are desired.
C Arrays are not passed through COMMON but passed as arguments to the
C subroutines.
C
      COMMON /SIZE/ NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,
1      NUMEQN,LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      INTEGER NUMANG,NUMRAD,NUMELM,INTNOD,NUMNOD,CODIAG,NUMEQN,
1      LENGTH,WIDTH,SPACE,BNDELM,BCOLS,ALENG,AWIDE,ATMPL
      COMMON /PROB/ W2,GA,GB,RO,EXTG,ALPHA,THETA0
      REAL W2,GA,GB,RO,EXTG,ALPHA,THETA0
      COMMON /MAP/ SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2,RATIO,GRADNT
      INTEGER RATIO
      REAL SWEEP,RANGE,DRAD,DANG,BDANG1,BDANG2
      LOGICAL GRADNT
      common /debug/ dmain,dmesh,dassm,dktest,dforce,
1      dhspac,drect,dtri,dgamma,dfilam,damat,dbmat,
1      dcmat,dnorm,ddiag,ddiag2,dfunc,dderiv,dctest,datest
      logical dmain,dmesh,dassm,dktest,dforce,dhspac,
1      drect,dtri,dgamma,dfilam,damat,dbmat,dcmat,dnorm,
1      ddiag,ddiag2,dfunc,dderiv,dctest,datest
C
C Dimension and declare arrays used within this subroutine.
C
      REAL B(NUMEQN,INTNOD)
      COMPLEX FG(INTNOD),FD(INTNOD),SLTN(INTNOD),W(INTNOD),LAM(BNDELM)
C
C Declare variables used only by this subroutine.
C
      INTEGER ROW,COL,COL1,COL2,PULL,IER,N,L,M,I,J,P
      REAL RAD,RE,IM,AMP,PHASE,AMPC,PHASEC,PHASC

```

```

      COMPLEX X,DUMMY
C
C Output boundary node displacements.
C
      WRITE(26,600)
      DO 120 ROW=1,INTNOD
        WRITE(26,500) ROW,SLTN(ROW),W(ROW)
120    CONTINUE
C
C Back substitute to determine surface node displacements.
C
      DO 130 I=2,NUMRAD
        ROW=INTNOD*(I-1)
        PUSH = NUMRAD+1-I
        FG(PUSH)=CMPLX(0.0,0.0)
        DO 140 COL=1,INTNOD
          FG(PUSH)=FG(PUSH)+B(ROW,COL)*SLTN(COL)
140    CONTINUE
        ROW=ROW-(INTNOD-1)
        PUSH=I-1
        FD(PUSH)=CMPLX(0.0,0.0)
        DO 150 COL=1,INTNOD
          FD(PUSH)=FD(PUSH)+B(ROW,COL)*SLTN(COL)
150    CONTINUE
130    CONTINUE
      ROW=NUMEQN
      PUSH=NUMRAD
      FD(PUSH)=CMPLX(0.0,0.0)
      DO 160 COL=1,INTNOD
        FD(PUSH)=FD(PUSH)+B(ROW,COL)*SLTN(COL)
160    CONTINUE
C
C Seperate real and imaginary parts of displacement and calculate
c amplitude and phase of origin.
C
      X = CMPLX(0.0,-1.0)
      RE = FD(NUMRAD)
      DUMMY = FD(NUMRAD) - RE
      DUMMY = X*DUMMY
      IM = DUMMY
      AMPC = SQRT(RE**2+IM**2)
      PHASEC = ATAN(IM/RE)
C
C Determine and output displacement, amplitude, phase with respect to
C incoming wave, and phase with respect to origin for the surface nodes.
C
      WRITE(26,800)
      RAD=RANGE
      RE = SLTN(1)
      DUMMY = SLTN(1) - RE
      DUMMY = X*DUMMY
      IM = DUMMY
      AMP = SQRT(RE**2+IM**2)
      PHASE = ATAN(IM/RE)
      PHASC = PHASE - PHASEC
      WRITE(26,700)RAD,SLTN(1),AMP,PHASE,PHASC
      DO 170 J=1,NUMRAD
        RAD=RANGE-DRAD*FLOAT(J)
        RE = FD(J)
        DUMMY = FD(J) - RE

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```

        DUMMY = X*DUMMY
        IM = DUMMY
        AMP = SQRT(RE**2+IM**2)
        PHASE = ATAN(IM/RE)
        PHASC = PHASE - PHASEC
        WRITE(26,700)RAD,FD(J),AMP,PHASE,PHASC
170  CONTINUE
        DO 180 J=1,NUMRAD-1
            RAD = -DRAD*FLOAT(J)
            RE = FG(J)
            DUMMY = FG(J) - RE
            DUMMY = X*DUMMY
            IM = DUMMY
            AMP = SQRT(RE**2+IM**2)
            PHASE = ATAN(IM/RE)
            PHASC = PHASE - PHASEC
            WRITE(26,700)RAD,FG(J),AMP,PHASE,PHASC
180  CONTINUE
        RAD= -RANGE
        RE = SLTN(INTNOD)
        DUMMY = SLTN(INTNOD) - RE
        DUMMY = X*DUMMY
        IM = DUMMY
        AMP = SQRT(RE**2+IM**2)
        PHASE = ATAN(IM/RE)
        PHASC = PHASE - PHASEC
        WRITE(26,700)RAD,SLTN(INTNOD),AMP,PHASEC,PHASC
C
C Output tractions at boundary elements.
C
        WRITE(26,900)
        DO 200 I=1,BNDELM
            WRITE(26,950)I,LAM(I)
200  CONTINUE
C
C Output format statements.
C
500  FORMAT(2X,I5,2X,E15.6,2X,E15.6,2X,E15.6,2X,E15.6)
600  FORMAT(/,2X,'***** BOUNDARY NODE DISPLACEMENTS
1    *****',//,
1    2X,18X,'SOLVED',26X,'FREE FIELD',/,
1    2X,' NODE',7X,'REAL',11X,'IMAGINARY',10X,'REAL',11X,'IMAGINARY')
700  FORMAT(4X,F5.2,2X,E15.6,2X,E15.6,2X,E15.6,2X,E15.6,2X,E15.6)
800  FORMAT(/,2X,'***** SURFACE NODE DISPLACEMENTS
1    *****',//,
1    3X,'RADIUS',7X,'REAL',13X,'IMAGINARY',8X,'AMPLITUDE',8X,'PHASE',
1    12X,'PHASE',/,67X,'FREE FIELD',7X,'CENTER')
950  FORMAT(4X,I5,2X,E15.6,2X,E15.6)
900  FORMAT(/,2X,'***** BOUNDARY ELEMENT TRACTIONS
1    *****',//,
1    2X,'ELEMENT',7X,'REAL',13X,'IMAGINARY')
        RETURN
        END

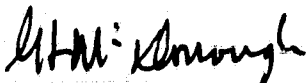
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APPROVAL

A NUMERICAL METHOD FOR INTERFACE PROBLEMS IN ELASTODYNAMICS

By David McGhee

The information in this report has been reviewed for technical content. Review of any information concerning Department of Defense or nuclear energy activities or programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.



G. F. McDONOUGH

Director, Systems Dynamics Laboratory